

SOUTHWEST RESEARCH INSTITUTE

EXPLORE MOON *to* MARS

Introduction to Additive Manufacturing for Propulsion and Energy Systems

Paul R. Gradl, Omar R. Mireles

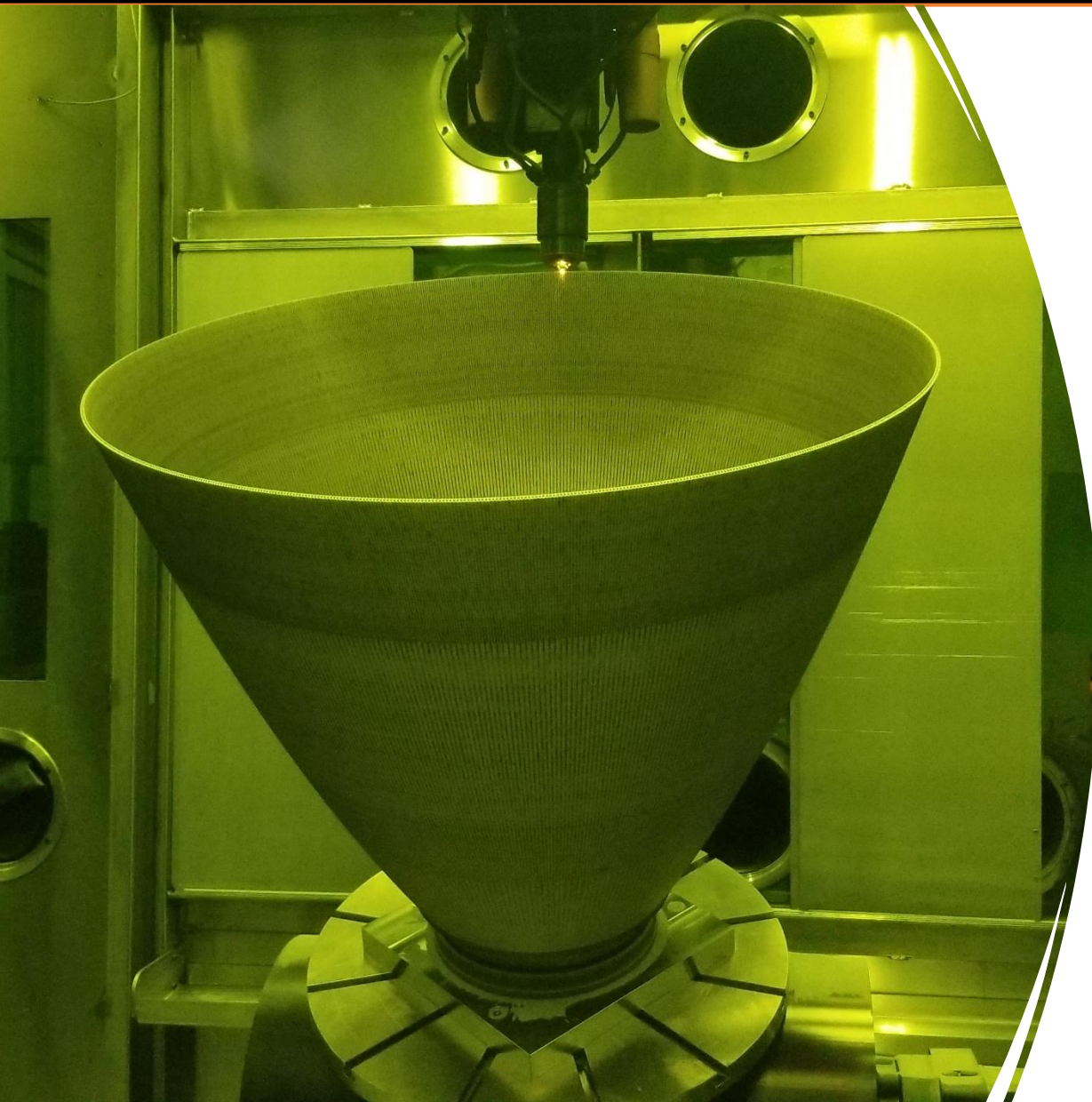
National Aeronautics and Space Administration (NASA)

Nathan Andrews

Southwest Research Institute

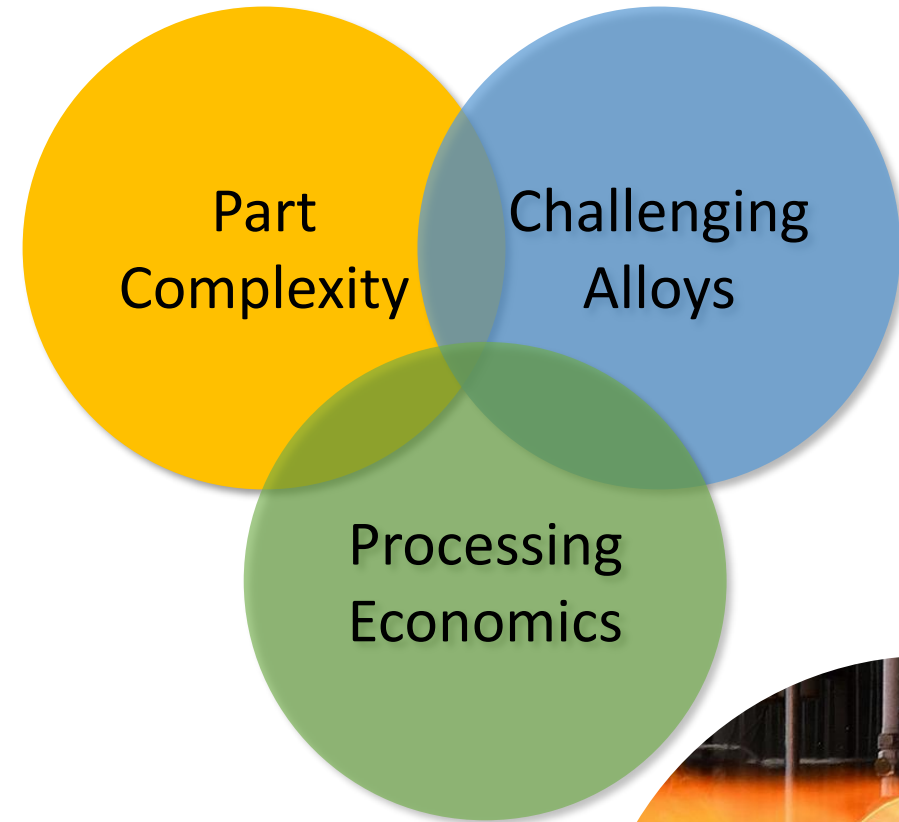
23 January 2023

AIAA SciTech

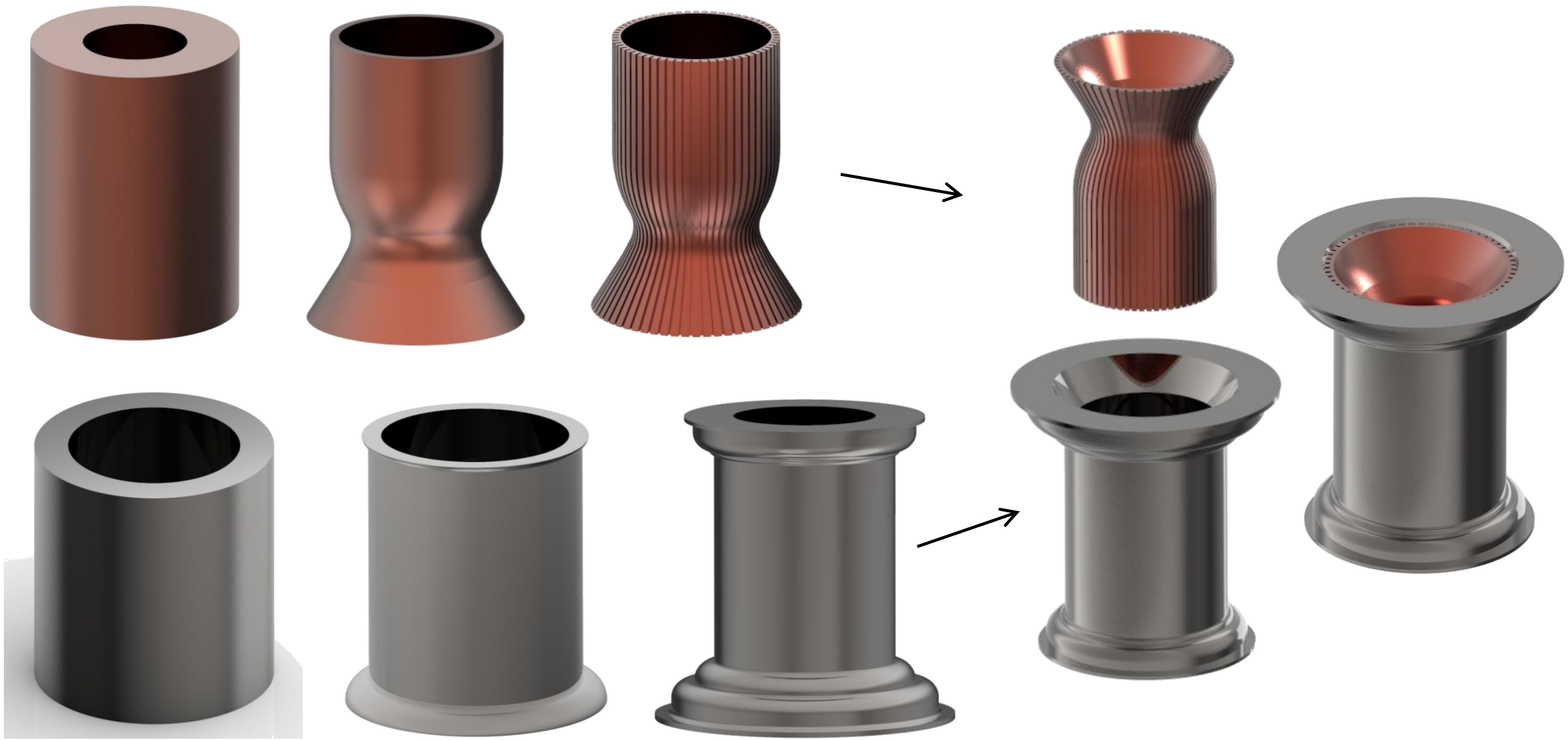


- Introduction
- Metal AM Process Selection
- Overview of AM Materials & Microstructure
- Metal AM Feedstock
- AM Post-Processing
- Design for the AM (DfAM) Lifecycle
- Example use cases

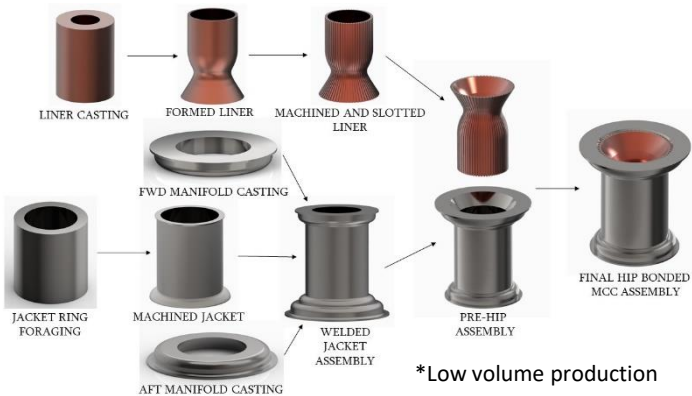
- Metal Additive Manufacturing (AM) can provide significant advantages for lead time and cost over traditional manufacturing for rocket engines.
 - Lead times reduced by 2-10x
 - Cost reduced by more than 50%
- Complexity is inherent in liquid rocket engines and AM provides new designs, part consolidation, and performance opportunities.
- Materials that are difficult to process using traditional techniques, long-lead, or not previously possible are now accessible using metal additive manufacturing.



Traditional Manufacturing...Forging to final assembly



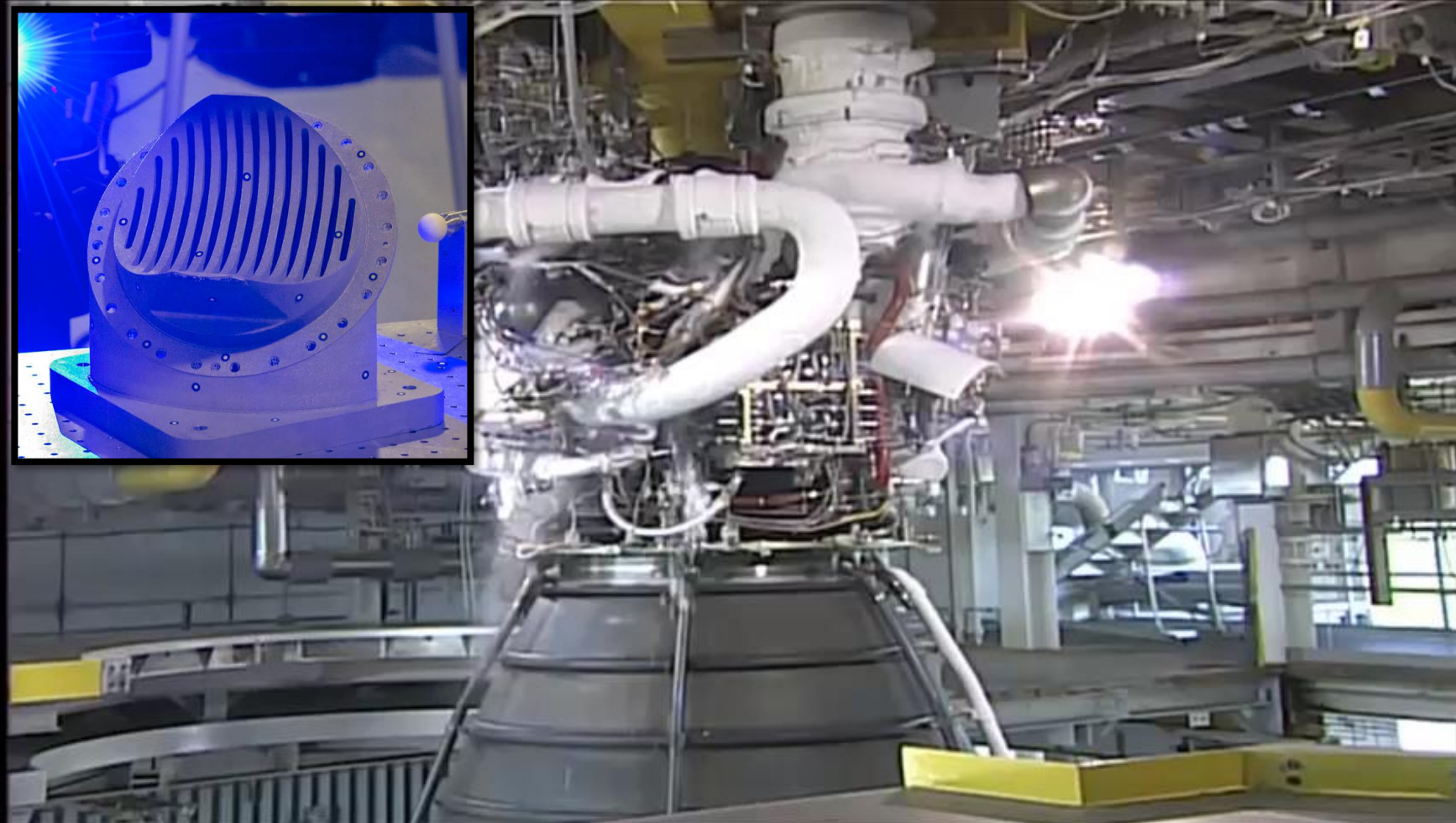
A rocket combustion chamber case study for AM



Category	Traditional Manufacturing	Initial AM Development	Evolving AM Development
Design and Manufacturing Approach	Multiple forgings, machining, slotting, and joining operations to complete a final multi-alloy chamber assembly	Four-piece assembly using multiple AM processes; limited by AM machine size. Two-piece L-PBF GRCop-84 liner and EBW-DED Inconel 625 jacket	Three-piece assembly with AM machine size restrictions reduced and industrialized. Multi-alloy processing; one-piece L-PBF GRCop-42 liner and Inconel 625 LP-DED jacket
Schedule (Reduction)	18 months	8 months (56%)	5 months (72%)
Cost (Reduction)	\$310,000	\$200,000 (35%)	\$125,000 (60%)

As AM process technologies evolve using multi-materials and processes, additional design and programmatic advantages are being discovered

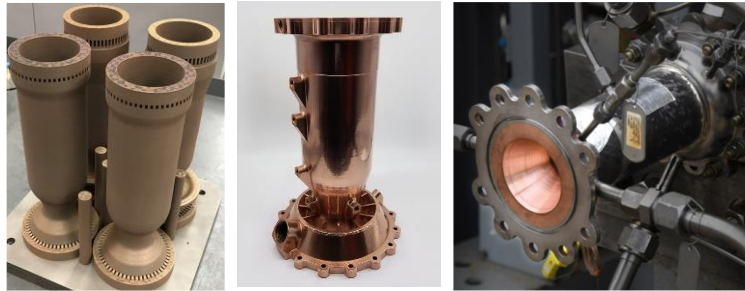
Additive Manufacturing in use on NASA Space Launch System (SLS)



**Successful hot-fire testing of full-scale additive manufacturing (AM) Part to be flown on SLS RS-25
RS-25 Pogo Z-Baffle – Used existing design with AM to reduce complexity from 127 welds to 4 welds**



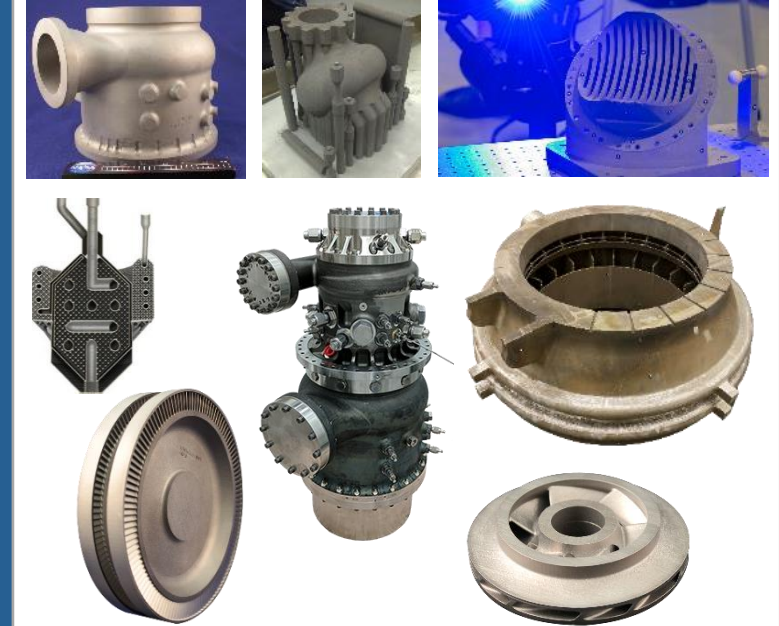
Additive Manufacturing (AM) Development at NASA for Liquid Rocket Engines



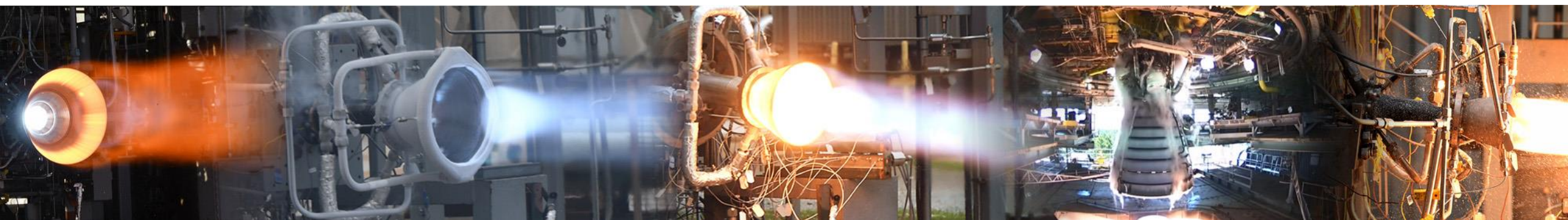
Laser Powder Bed Fusion (L-PBF)
Copper Alloys combined with other
AM processes to provide bimetallic



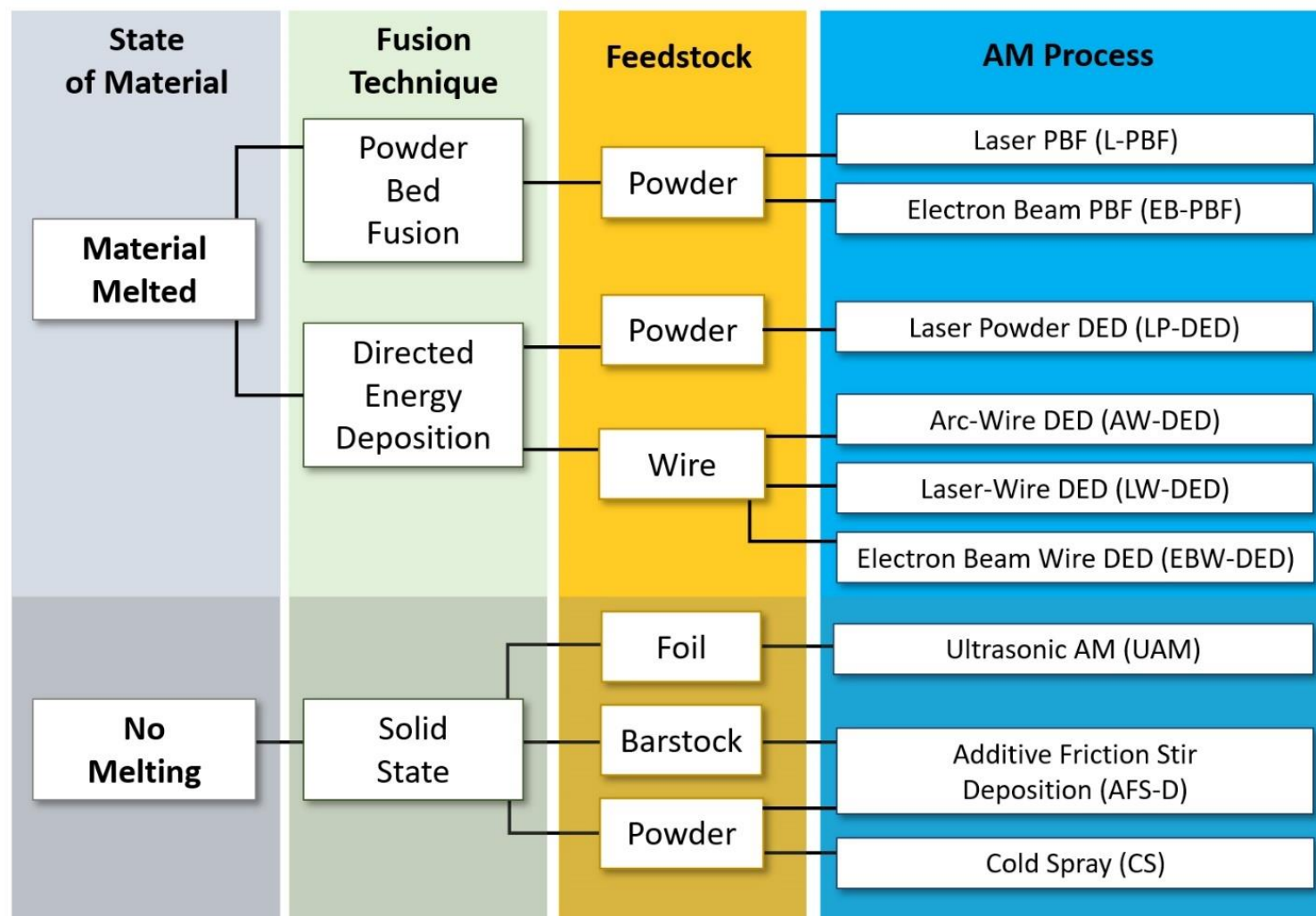
Directed Energy Deposition



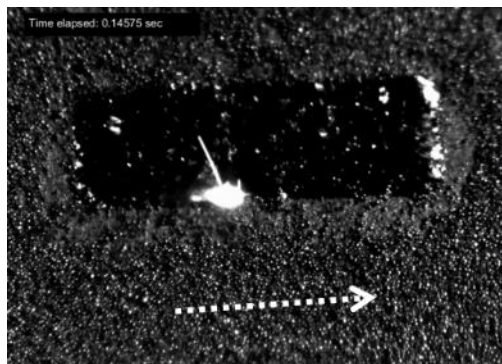
L-PBF of complex components, new
alloy developments for harsh
environment



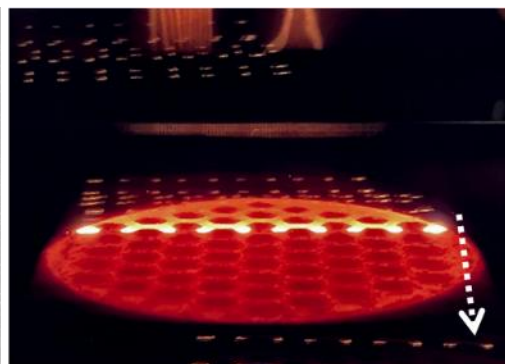
Various Metal AM Processes



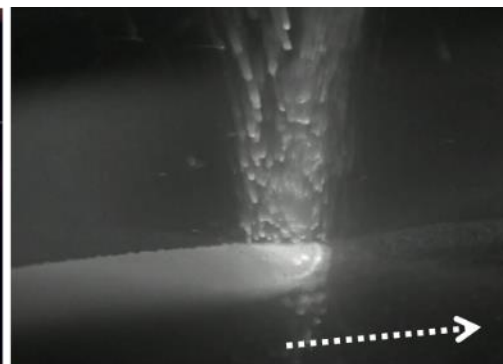
Many AM processes exists and must be traded (along with traditional techniques) to optimize



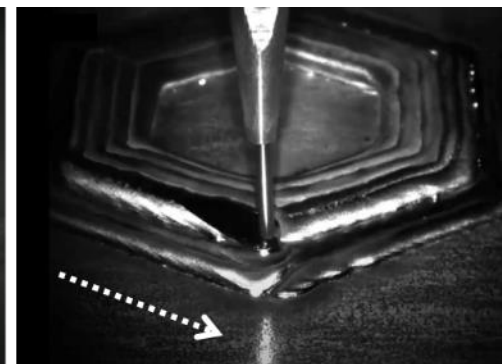
Laser Powder Bed Fusion



Electron Beam Powder Bed Fusion



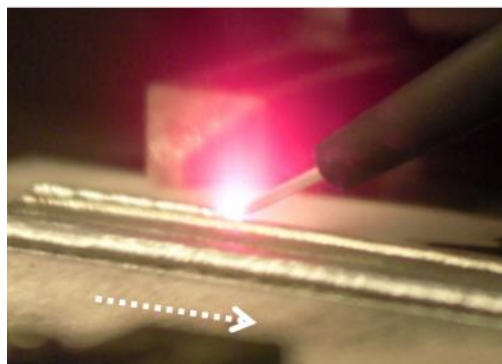
Laser Powder DED



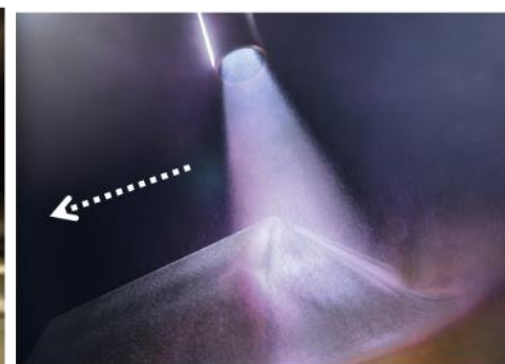
Laser Wire DED



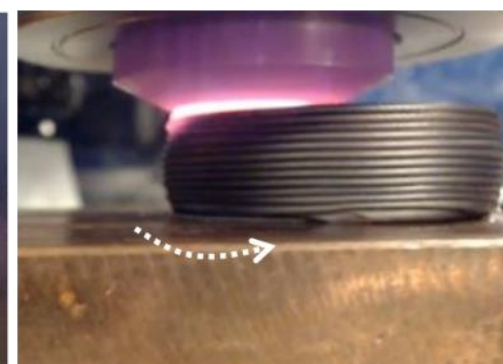
Arc Wire DED



Electron Beam Wire DED



Cold Spray



Additive Friction Stir Deposition



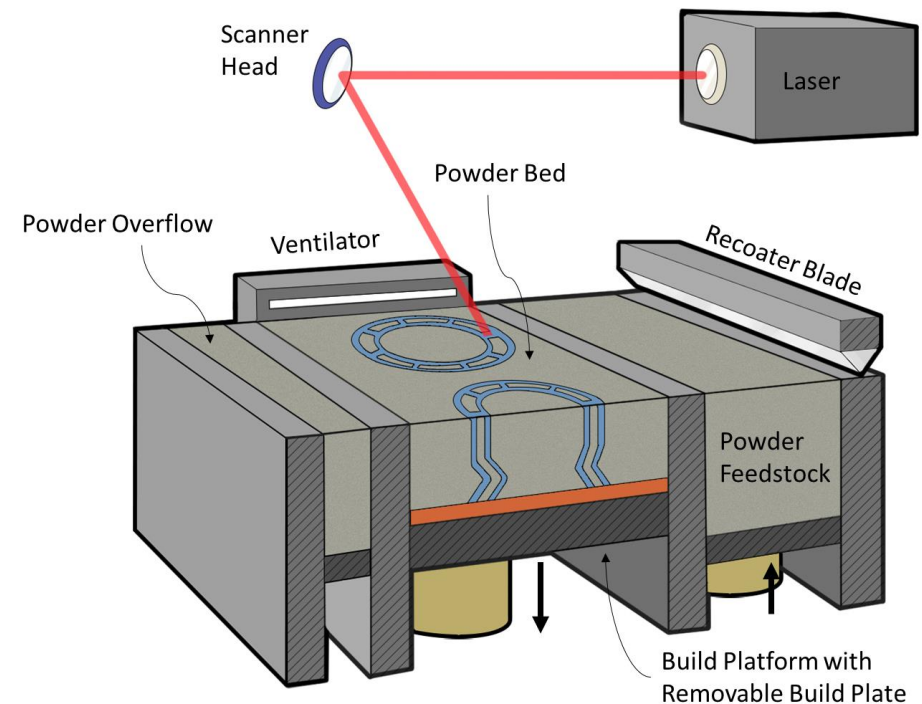
Ultrasonic Additive Manufacturing

**Not inclusive of all metal AM processes*

A) Laser Powder Bed Fusion [<https://doi.org/10.1016/j.actamat.2017.09.051>], B) Electron Beam Powder Bed Fusion [Credit: Courtesy of Freemelt AB, Sweden], C) Laser Powder DED [Credit: Formalloy], D) Laser Wire DED [Credit: Ramlab and Cavitar], E) Arc Wire DED [Credit: Institut Maupertuis and Cavitar], F) Electron Beam DED [NASA], G) Cold spray [Credit: LLNL], H) Additive Friction Stir Deposition [NASA], I) Ultrasonic AM [Credit: Fabrisonic].

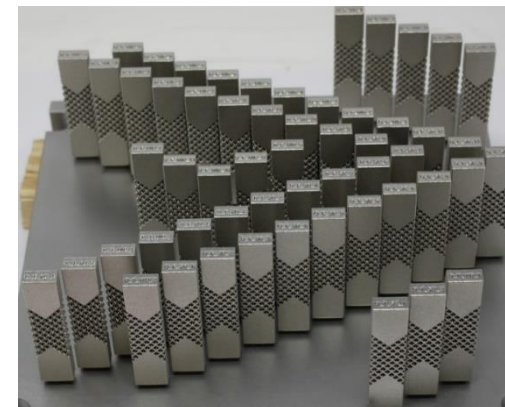
- **Laser Powder Bed Fusion (L-PBF)**

- Basic Process: Layer-by-layer powder-bed approach where desired features are melted using a laser and solidify.
- Advantages: High feature resolution, complex internal designs such as cooling channels.
- Disadvantages: Scale limited and does not provide a solution for all components.

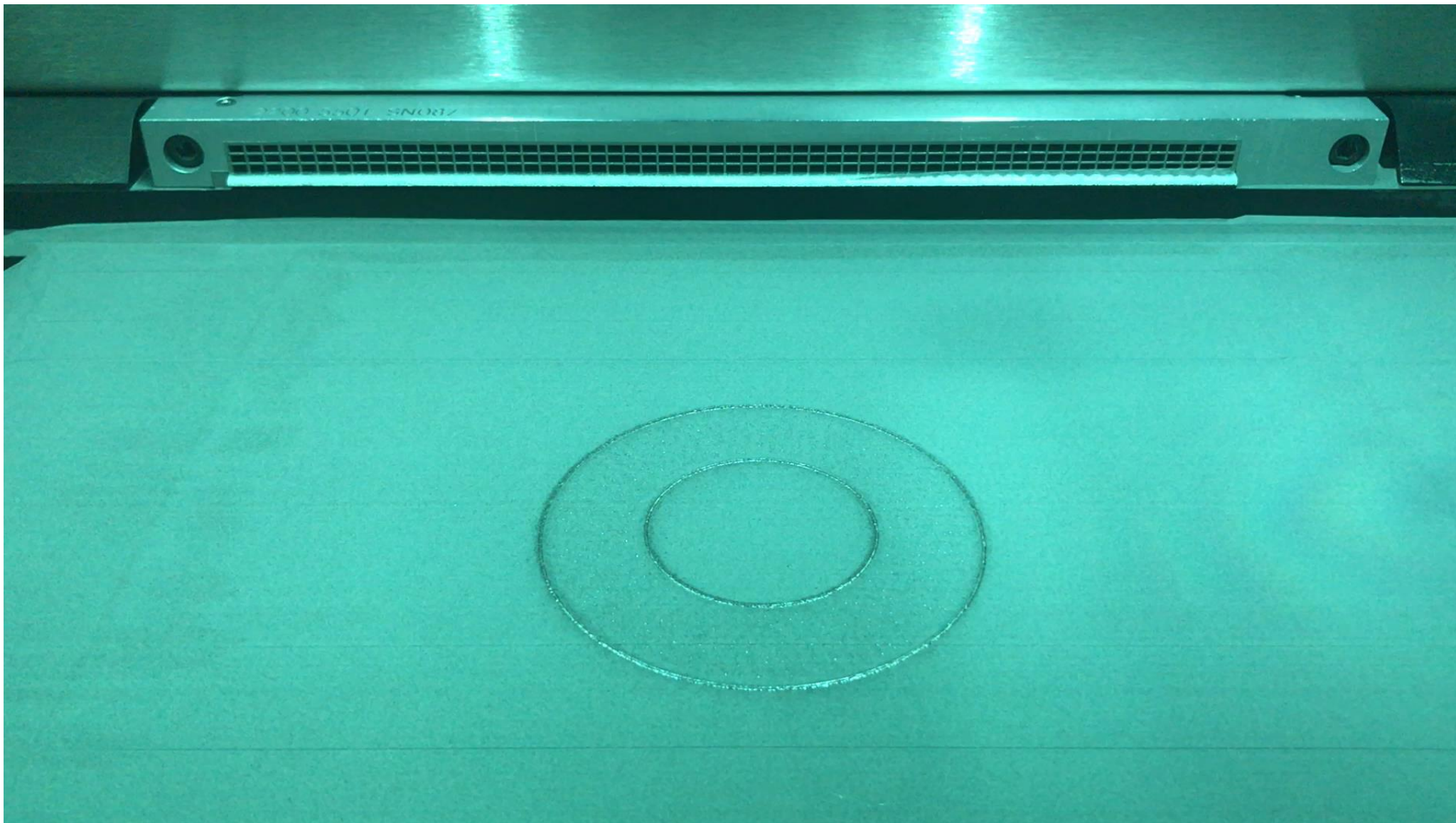


- **Electron Beam Melting**

- Basic Process: Similar to L-PBF but uses an electron beam.
- Advantages: Performed in-near vacuum, which is useful for reactive materials such as Ti6A4V.



Laser Powder Bed Fusion (L-PBF)

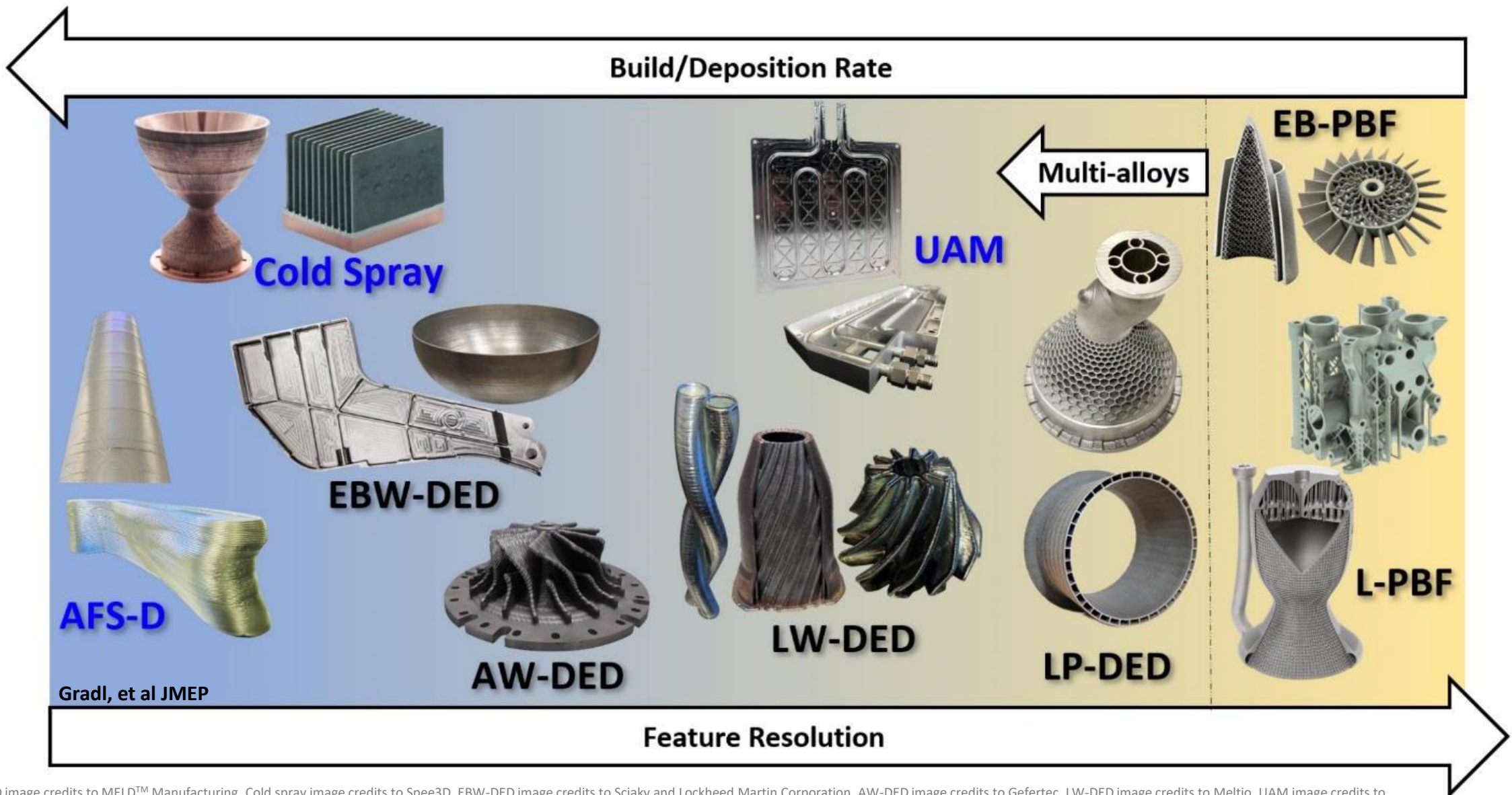




- What is the **alloy** required for the application?
- What is the **overall part size**?
- What is the **feature resolution** and internal **complexities**?
- Is it a **single alloy** or **multiple**?
- What are **programmatic requirements** such as cost, schedule, risk tolerance?
- What are the end-use environments and **properties required**?
- What is the **qualification/certification** path for the application/process?



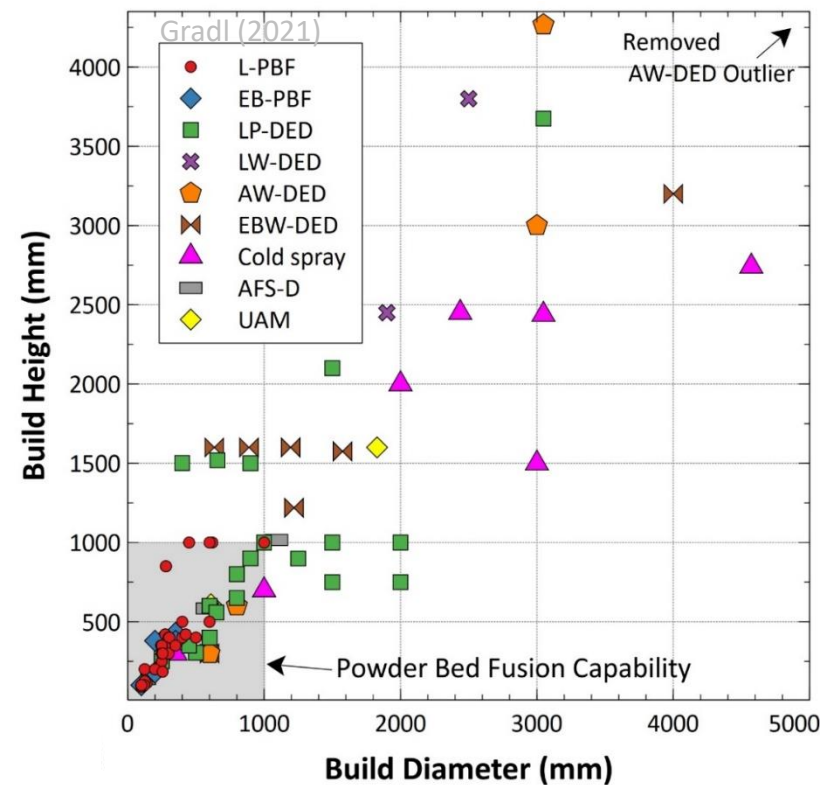
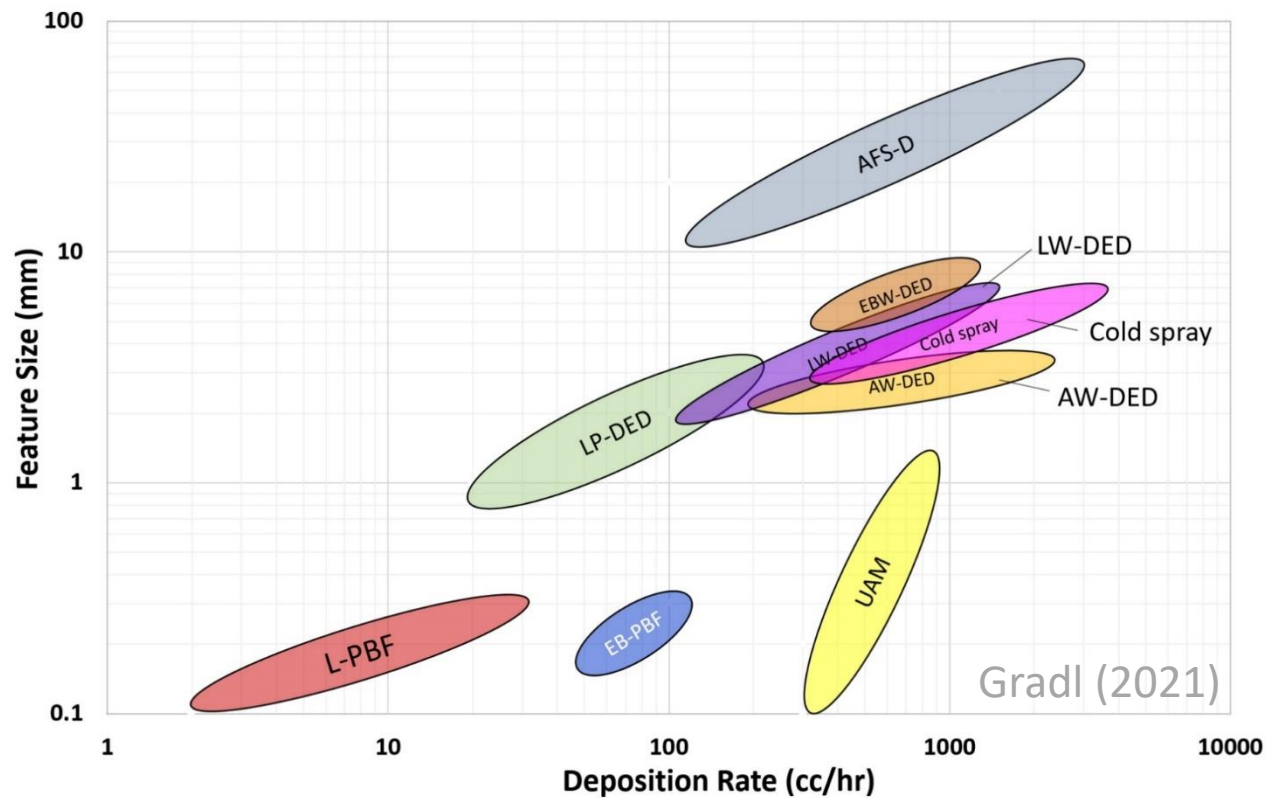
Criteria and Comparison Various Metal AM Processes



CREDITS: AFS-D image credits to MELD™ Manufacturing, Cold spray image credits to Spee3D, EBW-DED image credits to Sciaky and Lockheed Martin Corporation, AW-DED image credits to Gefertec, LW-DED image credits to Meltio, UAM image credits to Fabrisonic and NASA JPL, LP-DED image credits to DEPOZ project led by IRT Saint-Exupery and Formally, L-PBF image credits to Renishaw plc and CellCore GmbH/Sol Solutions Group AG, EB-PBF image credits to Wayland and GE Additive/Arcom.



Various criteria for selecting AM techniques



Complexity of Features

Scale of Hardware

Material Physics

Cost

Material Efficiency

Speed of Process

Material Properties

Internal Geometry

Availability

Post Processing

Large Scale Additive Manufacturing for Nozzles

SSME/RS-25

RL-10A-4

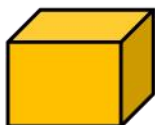
J-2X, Regen Only

RD-180

L-PBF Build
Boxes

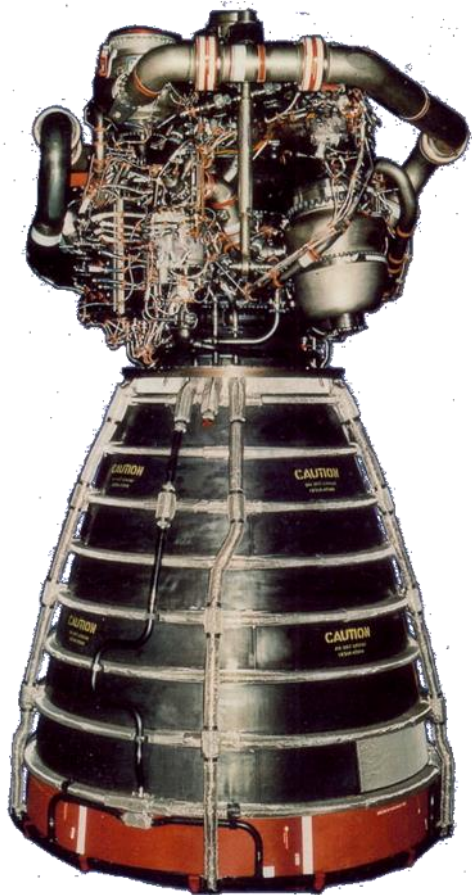


10x10x10



15.5x24x19

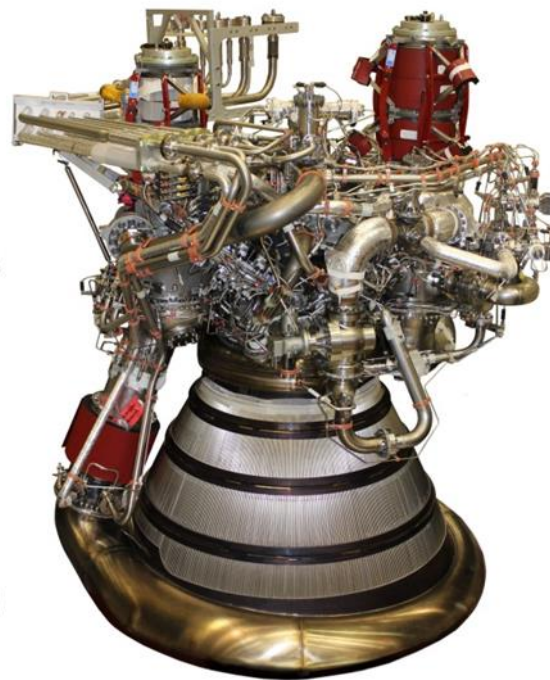
(inches)



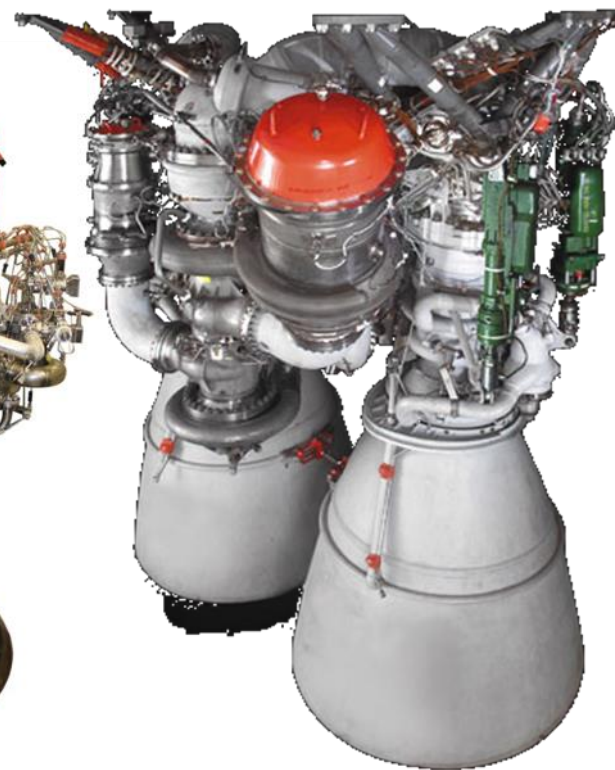
90"



46"



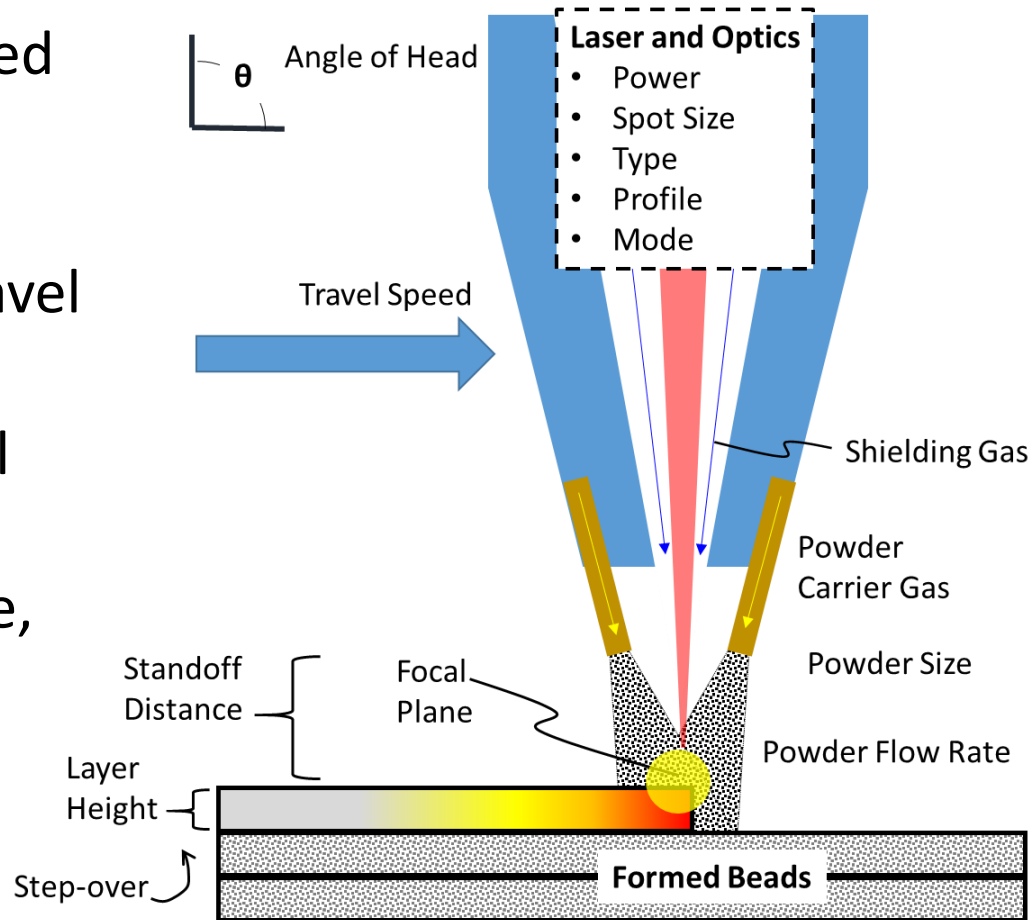
70"



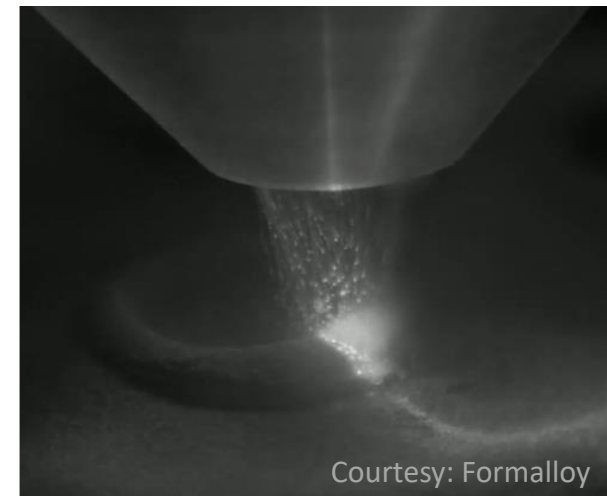
56"

Nozzle Exit Dia.

- Powder and laser beam path (sometimes optics) integrated into deposition head
- Basic parameters include power, powder feedrate, travel speed
- Additional geometry control for layer height, step over (hatching), standoff distance, angle of head and trunnion table
- Can vary spot size



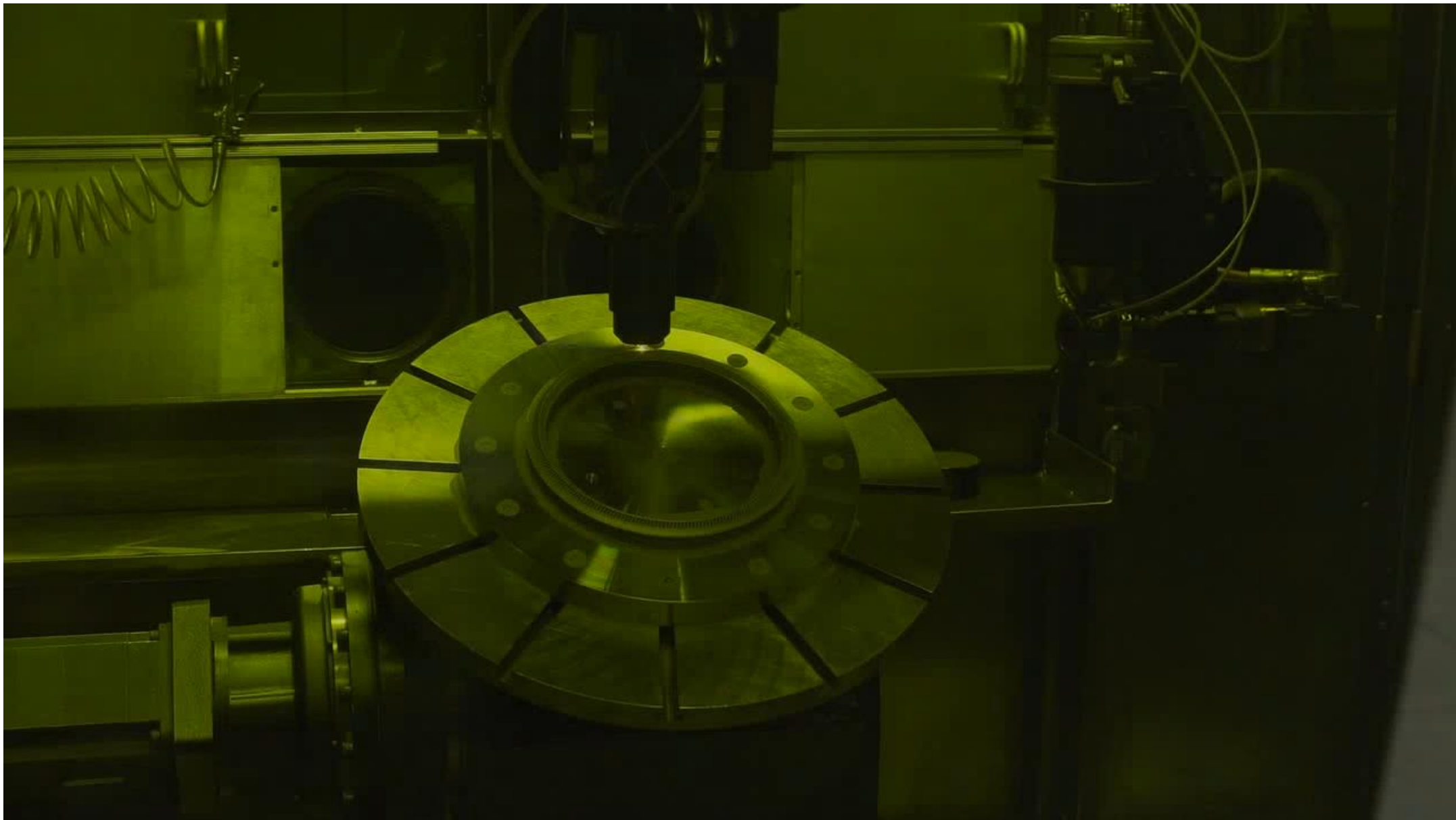
AIAA Book: Metal Additive Manufacturing for Propulsion Systems, Gradl, Protz, Mireles, Garcia (unreleased)



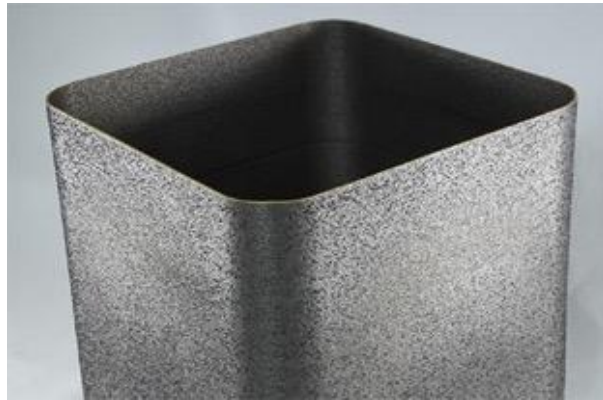
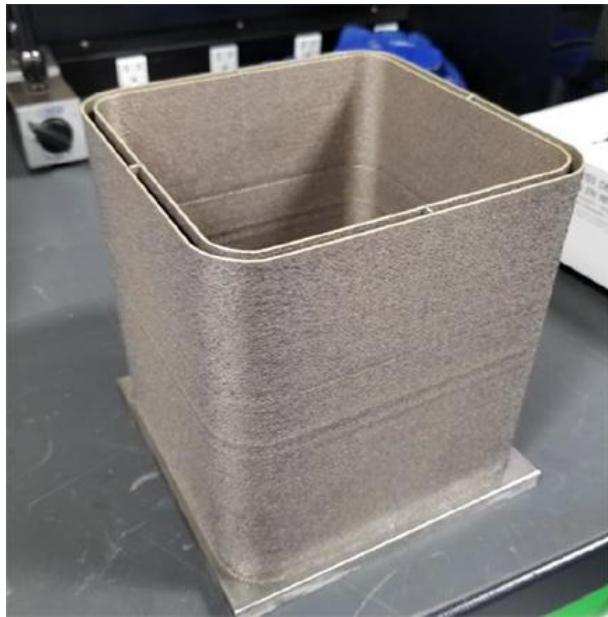
Laser Powder Directed Energy Deposition (DED)



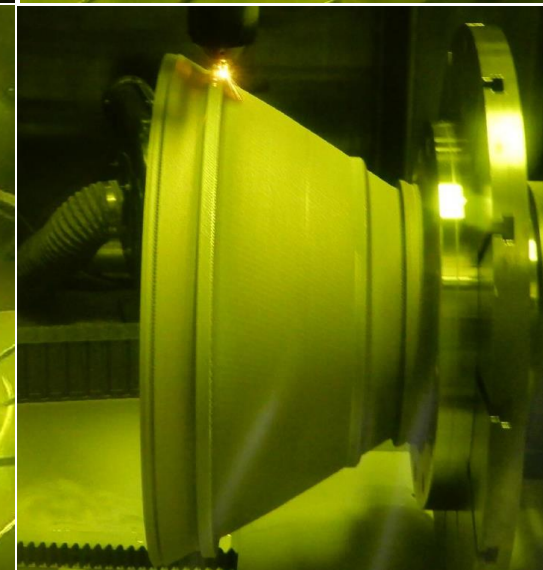
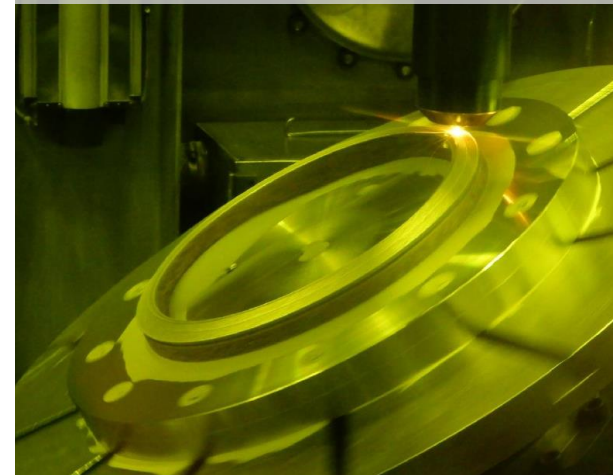
Example of LP-DED with small features



Large-scale Thin Wall Deposition of Nozzles



Process Development for DED of nozzles



LP-DED Large Scale Nozzle Development



NASA HR-1

60" (1.52 m) diameter and 70" (1.78 m) height with integral channels
90 day deposition



INNOVATIONS, INC.

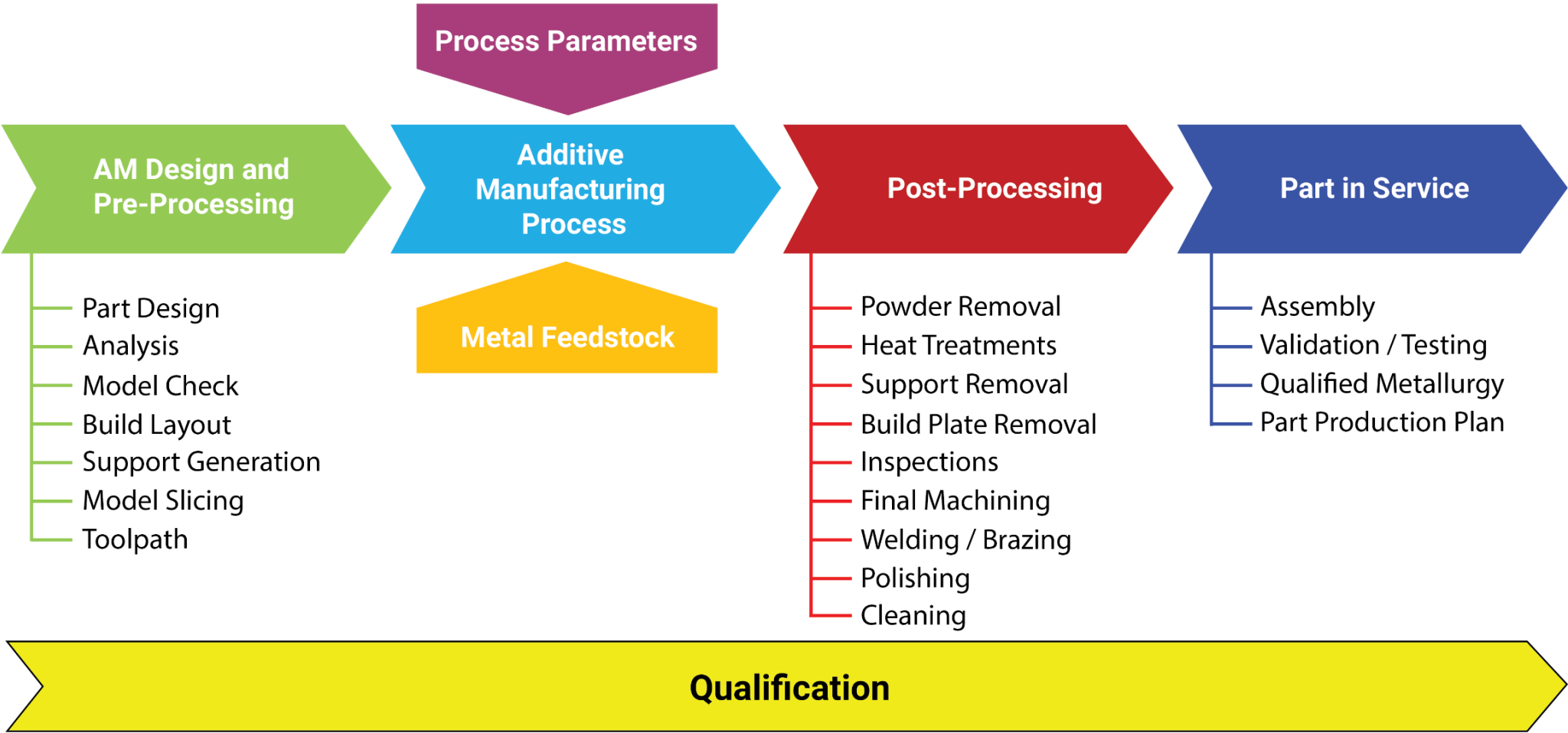


JBK-75

95" (2.41 m) dia and 111" (2.82 m) height
Near Net Shape Forging Replacement



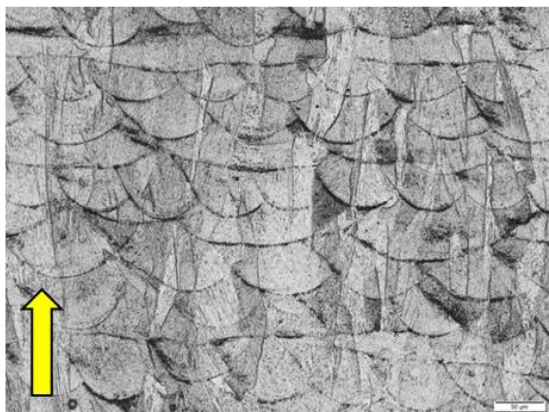
Additive Manufacturing Typical Process Flow



Proper AM process selection requires an integrated evaluation of all process lifecycle steps

Microstructure of Various AM Processes

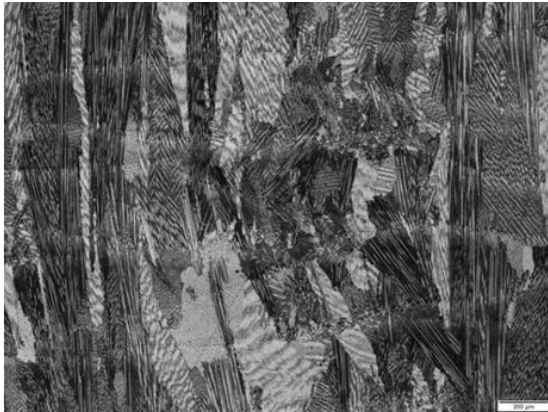
Alloy 625 – **As-Built**



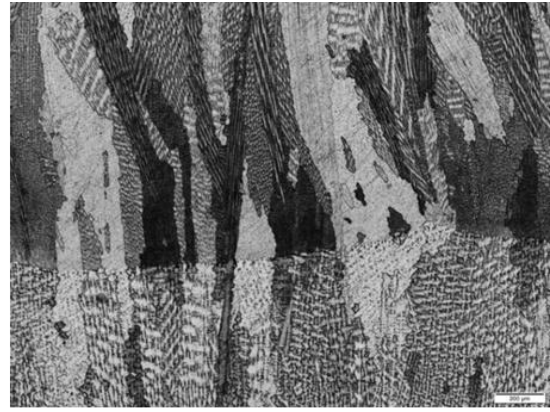
Laser Powder Bed Fusion



Electron Beam Powder Bed Fusion



Laser Powder DED (1070 W)



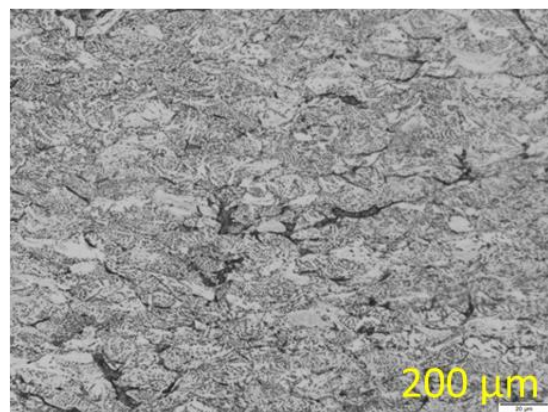
Electron Beam Wire DED



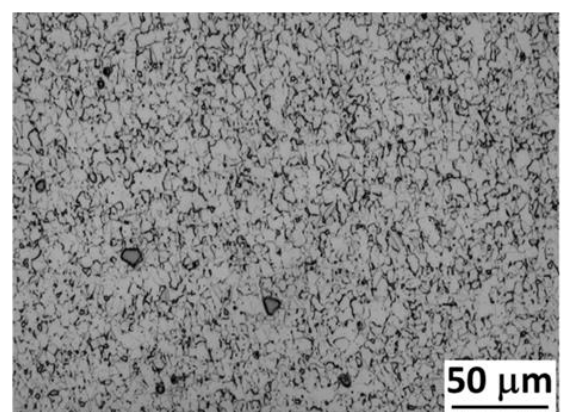
Laser Wire DED



Arc Wire DED



Cold Spray



Additive Friction Stir Deposition

Each AM process results in different grain structures, which ultimately influence properties

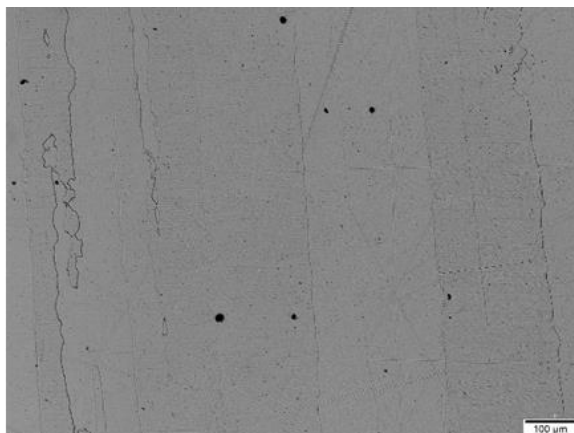
- Gamon, A., Arrieta, E., Gradl, P.R., Katsarelis, C., Murr, L.E., Wicker, R.B., Medina, F., 2021. Microstructure and hardness comparison of as-built Inconel 625 alloy following various additive manufacturing processes. Results in Materials 12. <https://doi.org/10.1016/j.rinma.2021.100239>
- Gradl, P., Tinker, D., Park, A., Mireles, O., Garcia, M., Wilkerson, R., McKinney, C., 2021. Robust Metal Additive Manufacturing Process Selection and Development for Aerospace Components. Journal of Materials Engineering and Performance, Springer. <https://doi.org/10.1007/s11665-022-06850-0>
- Rivera, O. G., Allison, P. G., Jordon, J. B., Rodriguez, O. L., Brewer, L. N., McClelland, Z., ... & Hardwick, N. (2017). Microstructures and mechanical behavior of Inconel 625 fabricated by solid-state additive manufacturing. Materials Science and Engineering: A, 694, 1-9.
- Image from Mark Norfolk, Fabrisonic

Microstructure of Various AM Processes

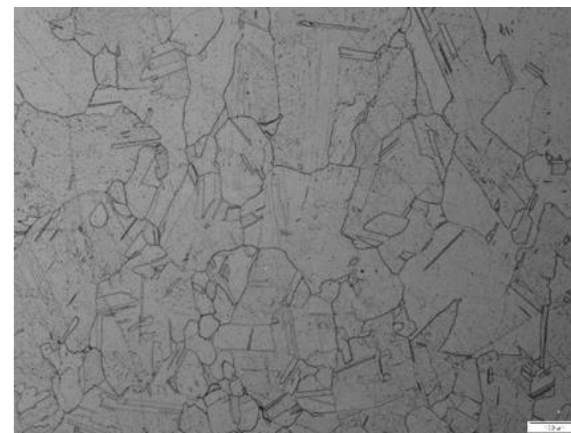
Alloy 625 – Stress Relief, HIP, Solution per AMS 7000



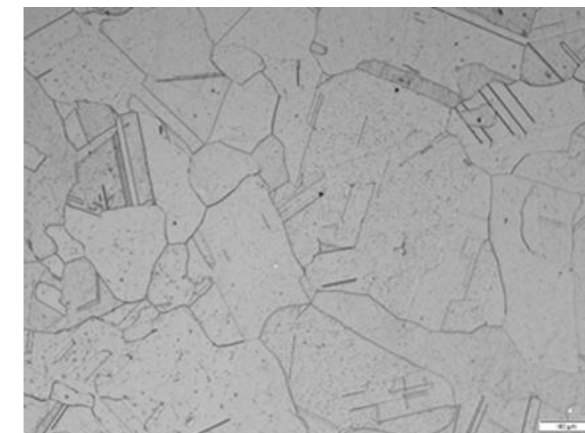
Laser Powder Bed Fusion



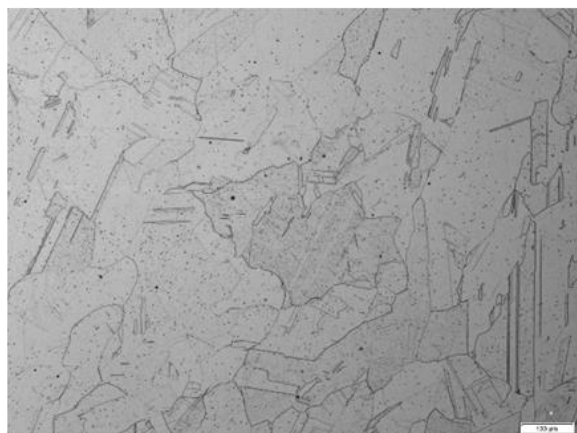
Electron Beam PBF



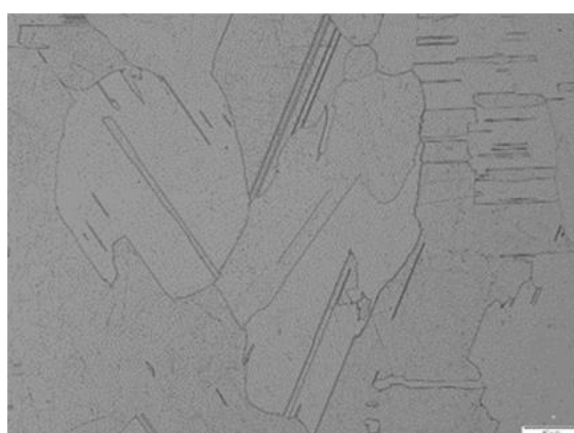
Laser Powder DED (1070 W)



Electron Beam Wire DED



Laser Wire DED



Arc Wire DED



Cold Spray

- Gamon, A., Arrieta, E., Gradl, P.R., Katsarelis, C., Murr, L.E., Wicker, R.B., Medina, F., 2021. Microstructure and hardness comparison of as-built Inconel 625 alloy following various additive manufacturing processes. Results in Materials 12. <https://doi.org/10.1016/j.rinma.2021.100239>
- Gradl, P., Tinker, D., Park, A., Mireles, O., Garcia, M., Wilkerson, R., McKinney, C., 2021. Robust Metal Additive Manufacturing Process Selection and Development for Aerospace Components. Journal of Materials Engineering and Performance, Springer. <https://doi.org/10.1007/s11665-022-06850-0>

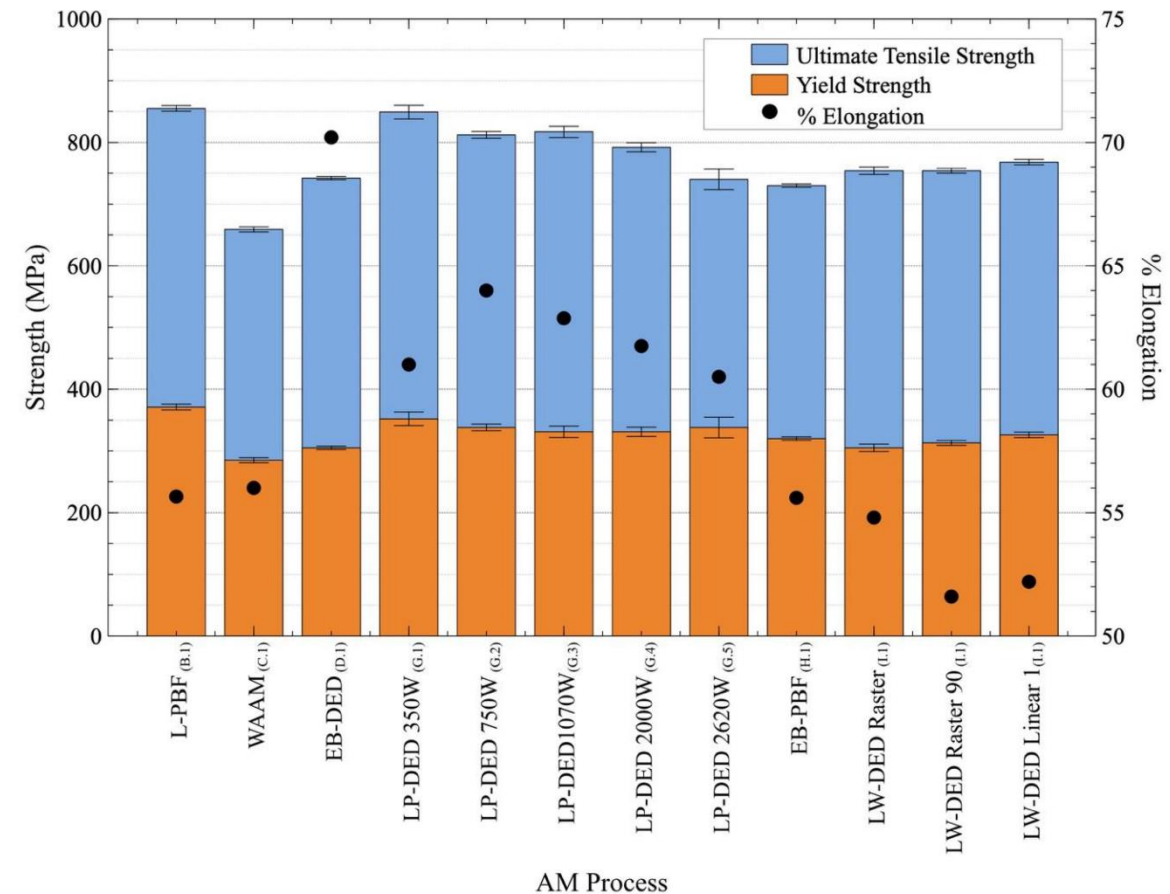


Material Properties for Various AM Processes



- Material properties are highly dependent on the type of process (L-PBF, DED, UAM, Cold spray....), the starting feedstock chemistry, the parameters used in the process, and the heat treatment processes used post-build.
- Each AM process results in different grain distributions, precipitates, and porosity, all of which influence final properties.
- Heat treatments should be developed based on the requirements and environment of the end component use.
- Process, parameters, and feedstock should all be stable before property development.

Alloy 625, Heat Treated per AMS 7000 Room Temperature UTS



***Not design data and provided as an example only**



AM Alloys and Processes In-work



Material ▼	Process ▼
Haynes 282	L-PBF
Haynes 282	LP-DED
Hastelloy X	L-PBF
Hastelloy X	LP-DED
Inconel 625	L-PBF
Inconel 625	LP-DED
Inconel 625	LW-DED
Inconel 625	AW-DED
Inconel 718	L-PBF
Inconel 718	LP-DED
Inconel 718	AW-DED
Inconel 939	L-PBF
Haynes 230	L-PBF
Haynes 230	LP-DED
Haynes 214	L-PBF
Haynes 233	L-PBF
Haynes 233	LP-DED

Material ▼	Process ▼
NASA HR-1	L-PBF
NASA HR-1	LP-DED
JBK-75	L-PBF
JBK-75	LP-DED
CoCr	L-PBF
CoCr	LP-DED
Invar 36	LP-DED
Stellite 21	LP-DED
316L	LP-DED
15-5	LP-DED
17-4	L-PBF
17-4	LP-DED
Scalmalloy	L-PBF
6061-RAM2	L-PBF
6061-RAM2	LP-DED
F357	L-PBF
F357	LP-DED
1000-RAM10	L-PBF
AlSi10Mg	L-PBF
AlSi10Mg	LP-DED
7A77	L-PBF

Material ▼	Process ▼
Monel K500	LP-DED
Monel K500	L-PBF
GRCo-42	L-PBF
GRCo-42	LP-DED
GRCo-84	L-PBF
C-18150	L-PBF
Ti6Al-4V	L-PBF
Ti6Al-4V	LP-DED
Ti6Al-4V	LW-DED
Ti6Al-4V	EBW-DED
Ti6242	L-PBF
Ti6242	LP-DED
GRX-810	L-PBF
GRX-810	LP-DED
Haynes 214-ODS	L-PBF
C-103	LP-DED

55+ Alloys in characterization



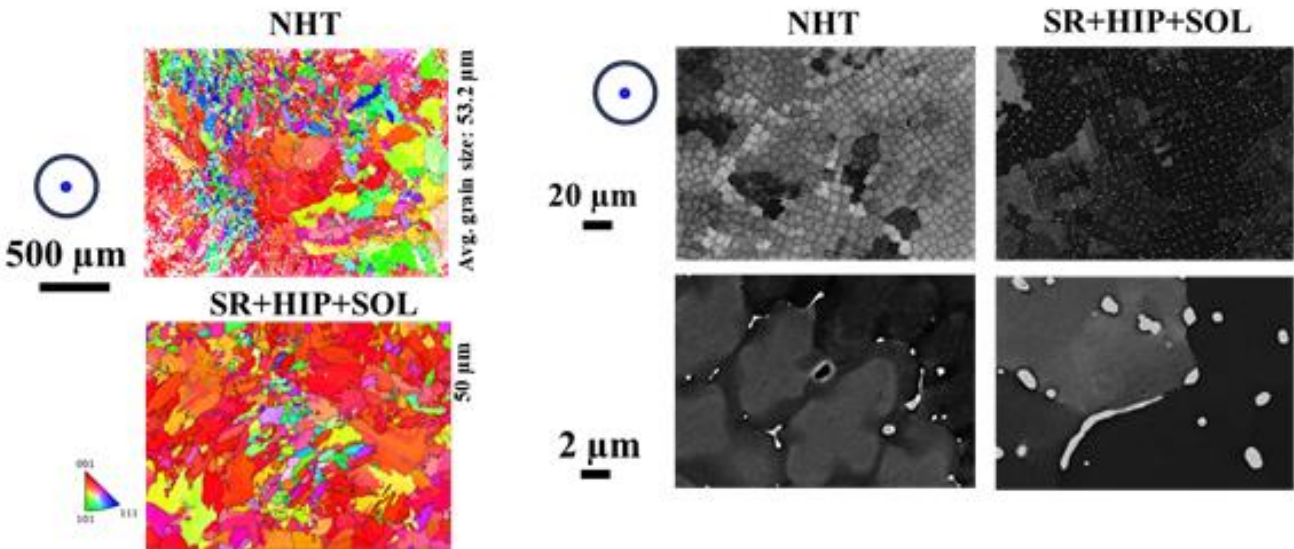
Data example of Haynes 230 LP-DED



Power (W)	Layer height (μm)	Travel speed (mm/min)	Powder feed rate (g/min)
1070	381	1016	19.10

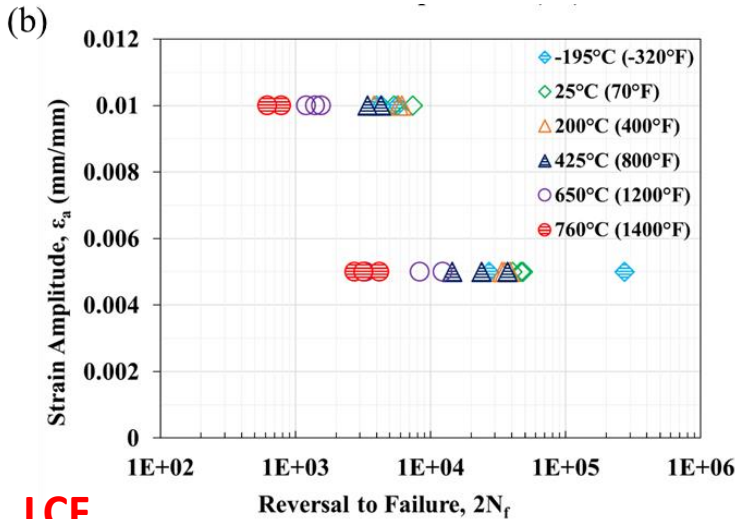
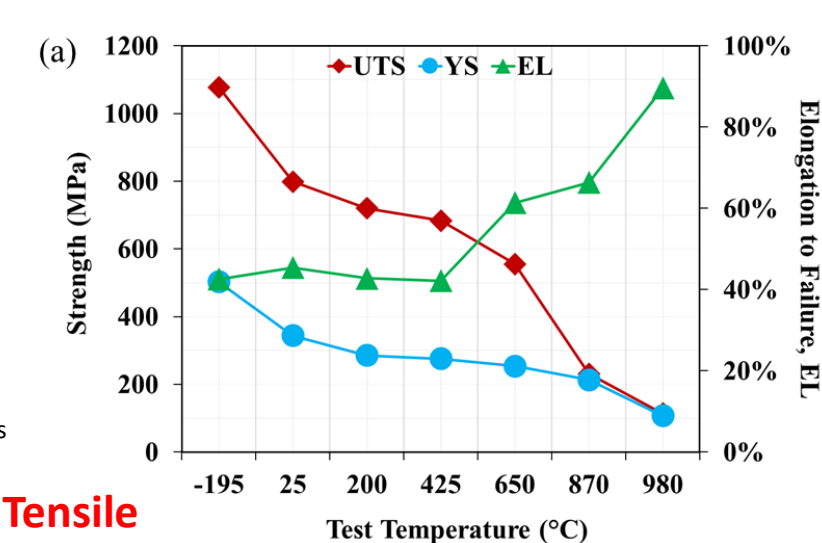
Procedure (Designation)	Temperature (°C)	Time (hrs)	Cooling
Stress Relief (SR)	1066	1.5	Furnace cool
HIP [2]	1163/103 MPa	3	Furnace cool
Solution Annealing (SOL)	1177	3	Argon quench

As-Built
Full Heat Treated

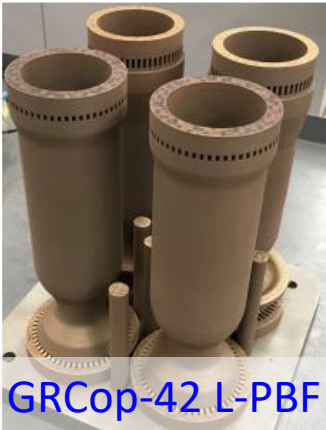


[2] HIP per ASTM F3301

Data from Gradl, Mireles, Protz, Garcia. “Metal Additive Manufacturing for Propulsion Applications”, AIAA Progress Series. (2022). Appendix A.



Max. Use Temp. (°C)	Alloy Family	Purpose	Novel AM Alloys	Propulsion Use
200	Aluminum	Light weighting	-	Various
750	Copper	High conductivity; strength at temperature	GRCop-42 GRCop-84	Combustion Chambers
800	Iron-Nickel	High strength and hydrogen resistance	NASA HR-1	Nozzles, Powerheads
900	Nickel	High strength to weight	-	Injectors, Turbines
1100	ODS Nickel	High strength at elevated temp; reduced creep	GRX-810 Alloy 718-ODS	Injectors, Turbines
1850	Refractory	Extreme temperature	C-103, C-103-CDS, Mo, W	Uncooled Chambers



GRCop-42 L-PBF



NASA HR-1 LP-DED



GRX-810
L-PBF

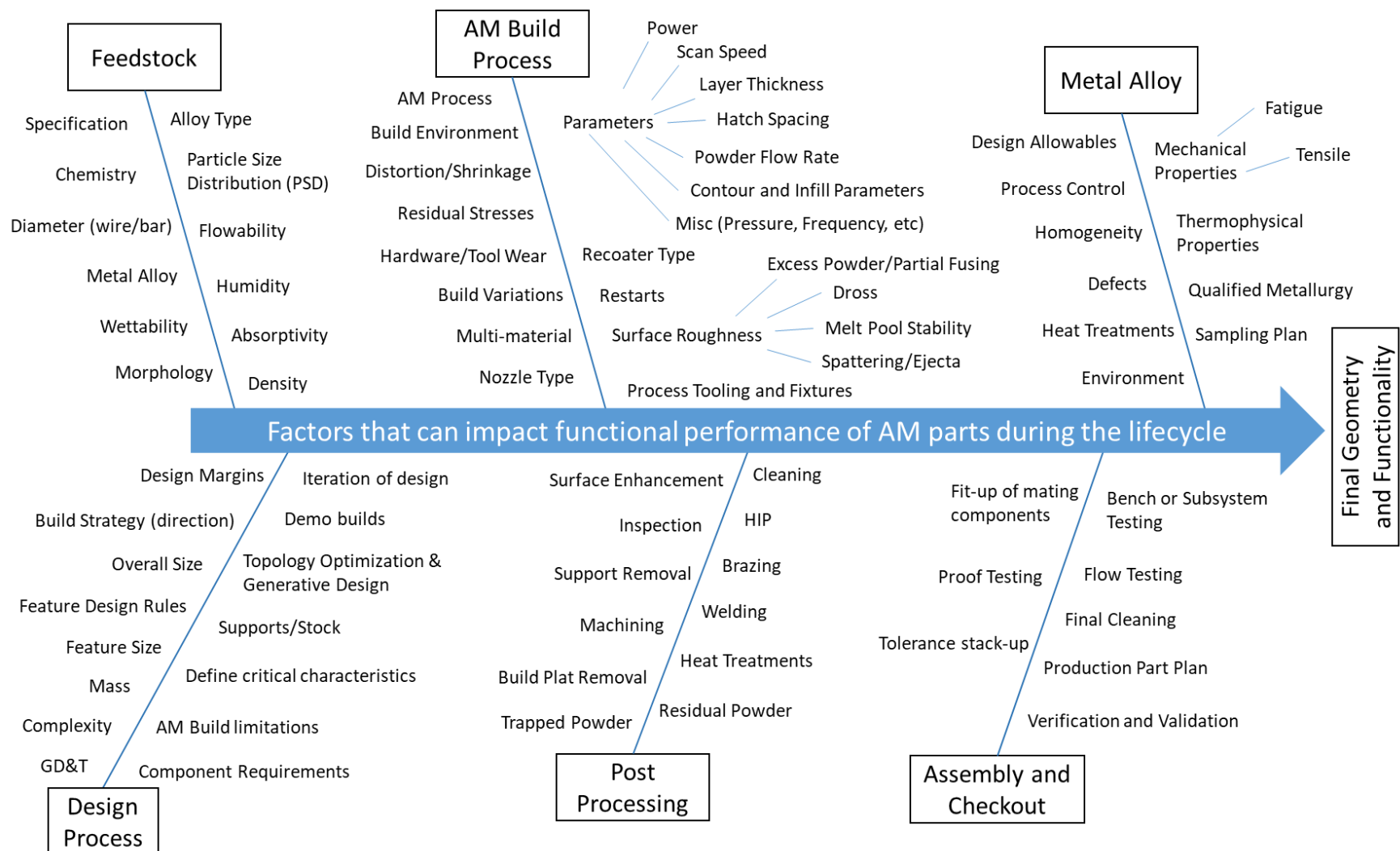


C103
L-PBF

New alloy development using various additive manufacturing processes (PBF and DED) can yield performance improvements over traditional alloys



The Challenges with AM Processes



There are a lot of inputs and steps in the AM lifecycle that must go right to meet the expected geometry



LP-DED Jacket



Cold spray Jacket

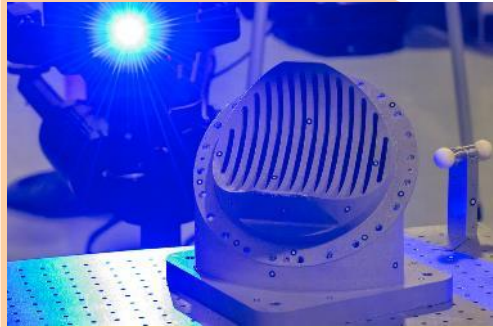


Direct deposit LP-DED nozzle
(Axial Bimetallic)



EBW-DED Jacket

Industrial Maturity and TRL of AM Processes



L-PBF

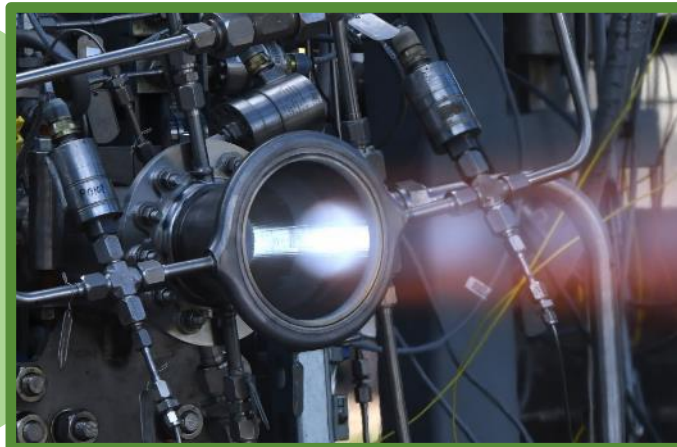


Cold spray

LP-DED



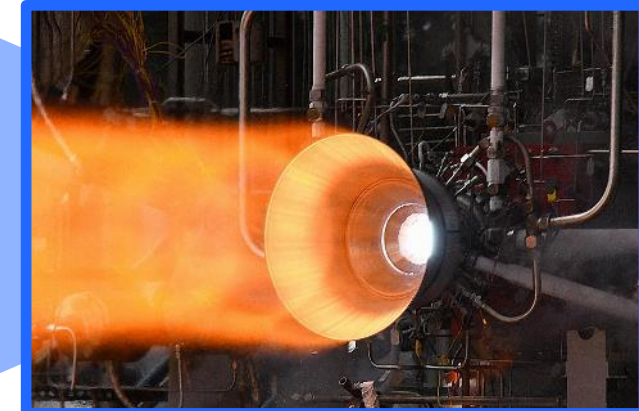
L-PBF



L-PBF



EBW-DED

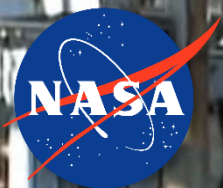


AW-DED



LW-DED

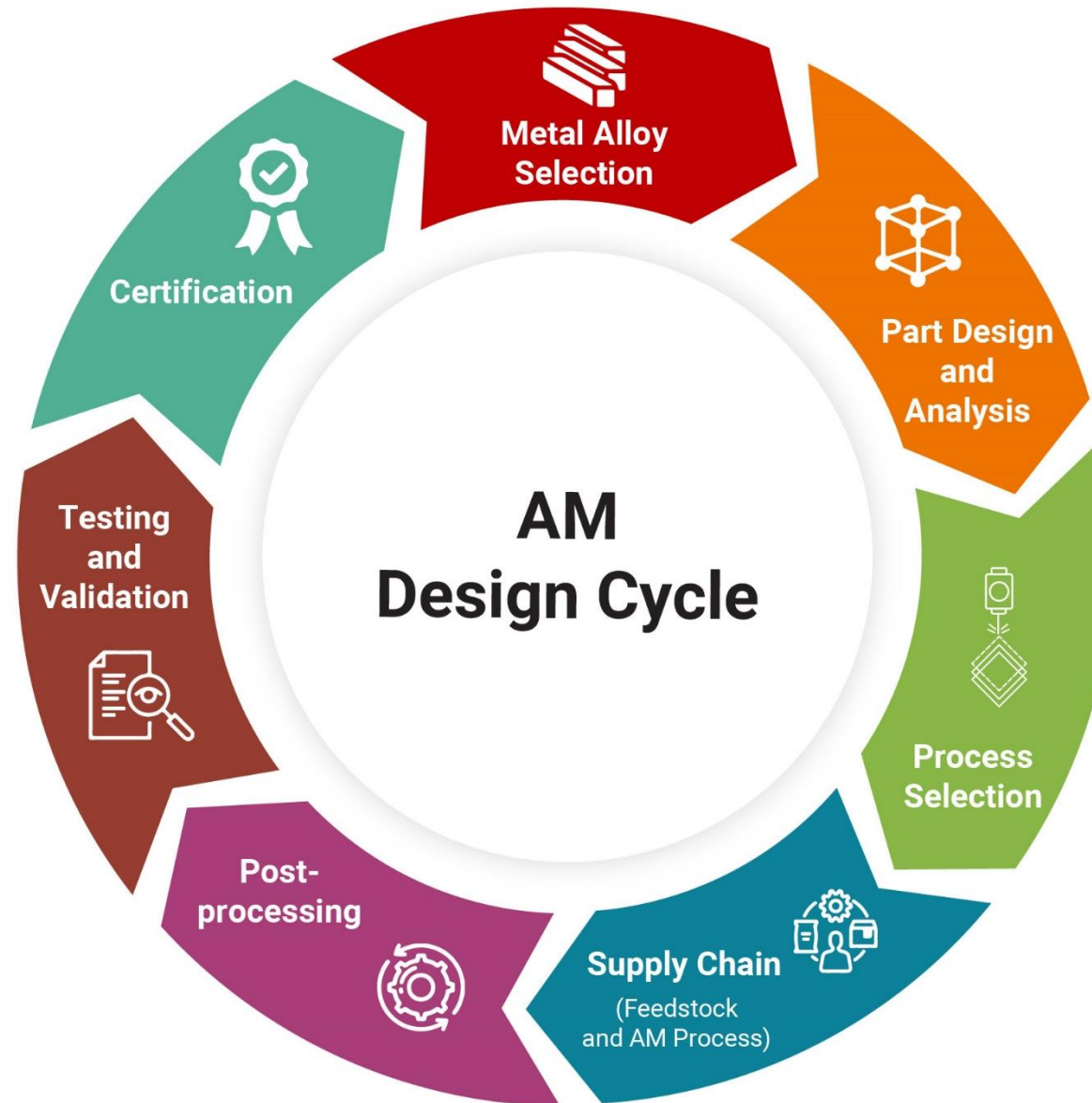
3/2/2018 3:23:08 PM



15:23:08



Design for Additive Manufacturing (DfAM)



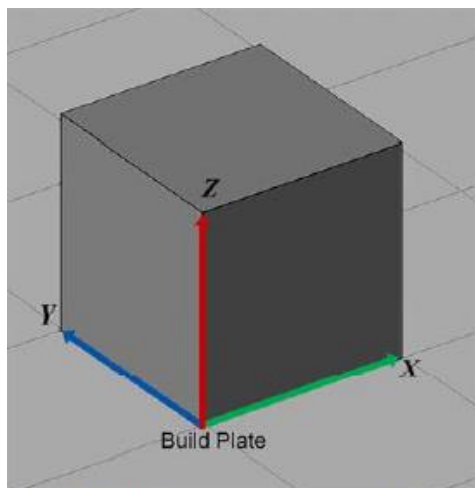


Fig. 7.1 AM reference coordinate system.

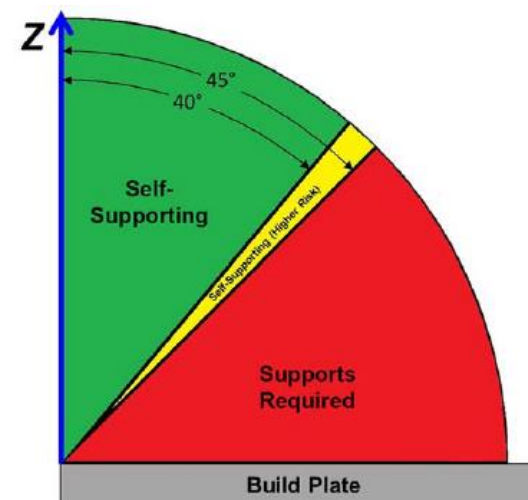


Fig. 7.14 Example of overhang surfaces in reference to the build plate and build direction (Z).

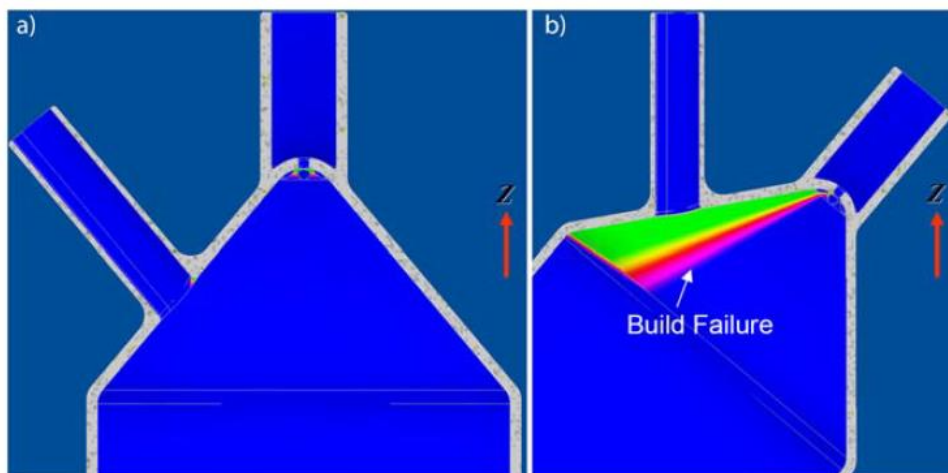


Fig. 7.16 Unsupported overhang surfaces vs. build direction. a) No unsupported surfaces. b) Unsupported surfaces.



Angle is measured in relation to the build direction, Z

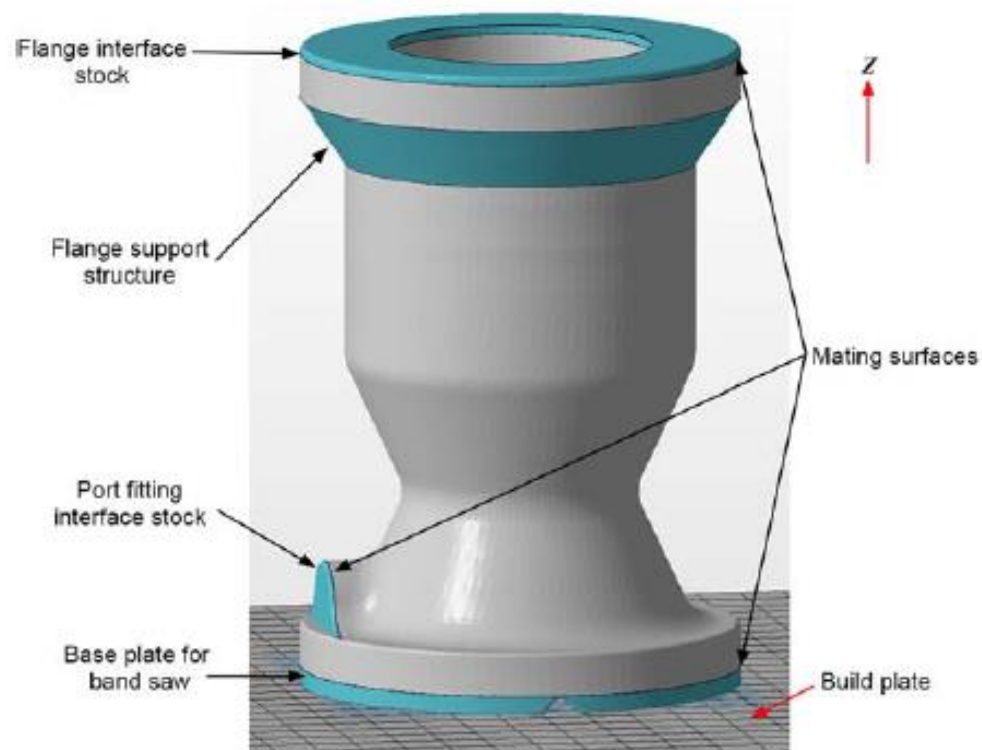


Fig. 7.11 Chamber design for L-PBF AM with sacrificial stock material added (turquoise regions).

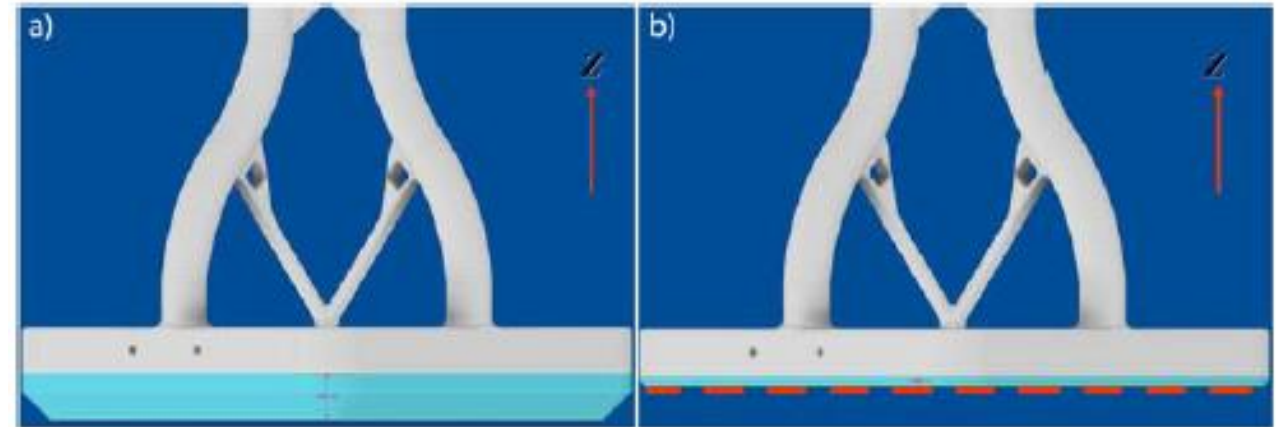


Fig. 7.13 Base-plate thickness vs. removal method for a) vertical band saw [5 mm (0.196 in.)] and b) wire-EDM [1 mm (0.039 in.)].

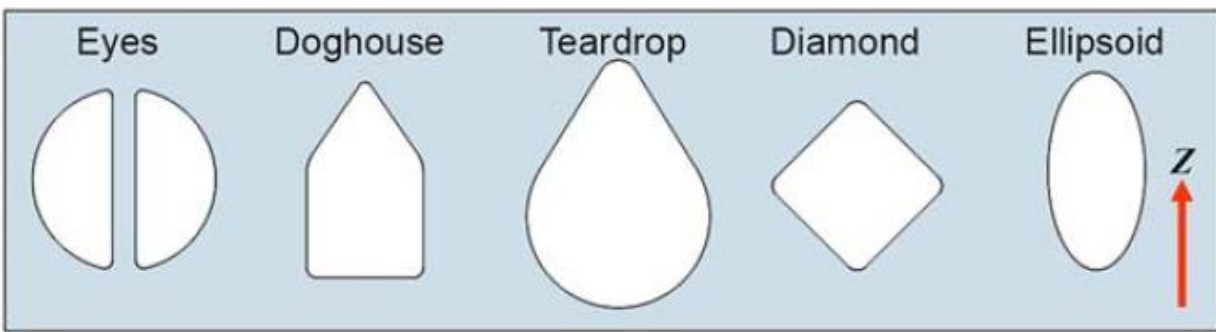


Fig. 7.18 Build failure observed at the tops of Ti6Al4V L-PBF holes oriented perpendicular to the build direction.

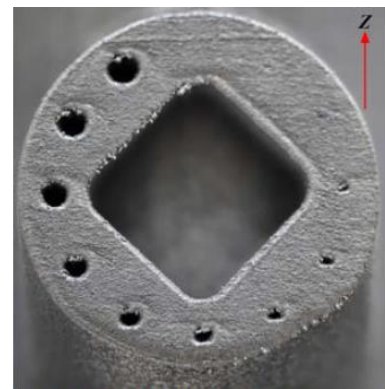


Fig. 7.20 Hole shape vs size, diamond slot, and surface roughness vs angle in L-PBF–built AISi10Mg.

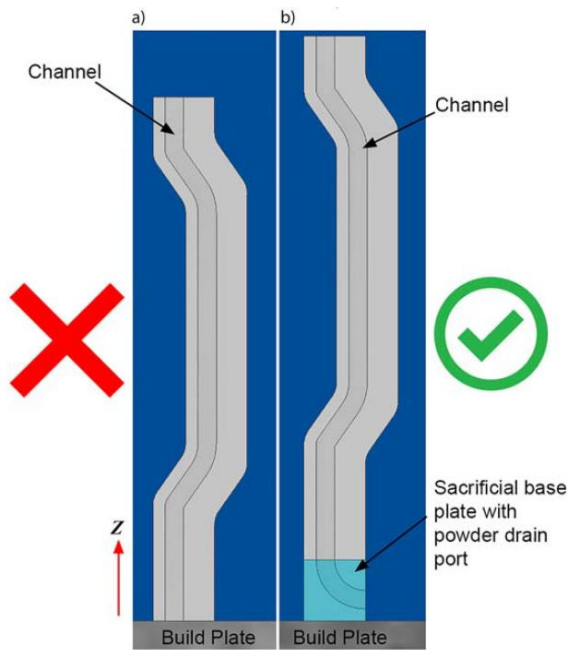


Fig. 7.26 a) Channel terminating at the build plate and b) base plate with powder drain port.

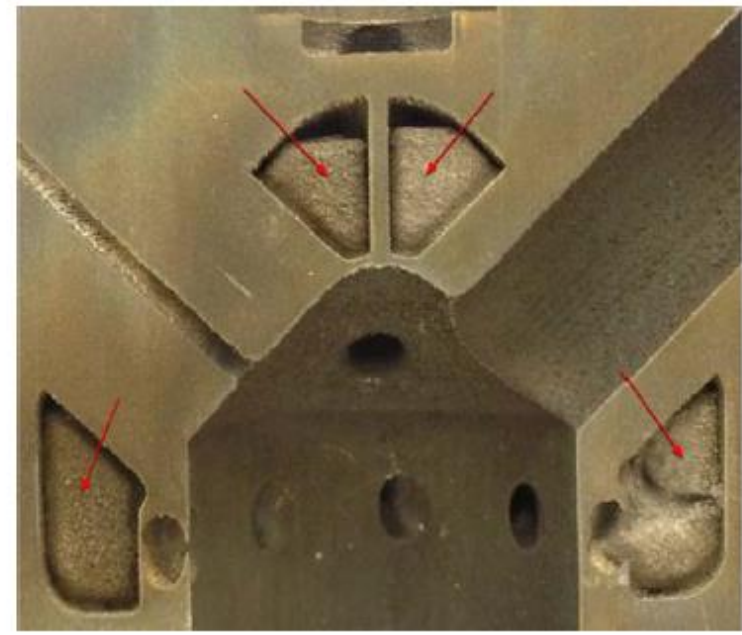


Fig. 5.5 Cross-sectional cut of a part with trapped powder that sintered during stress-relief heat treatment. (Source: NASA.)

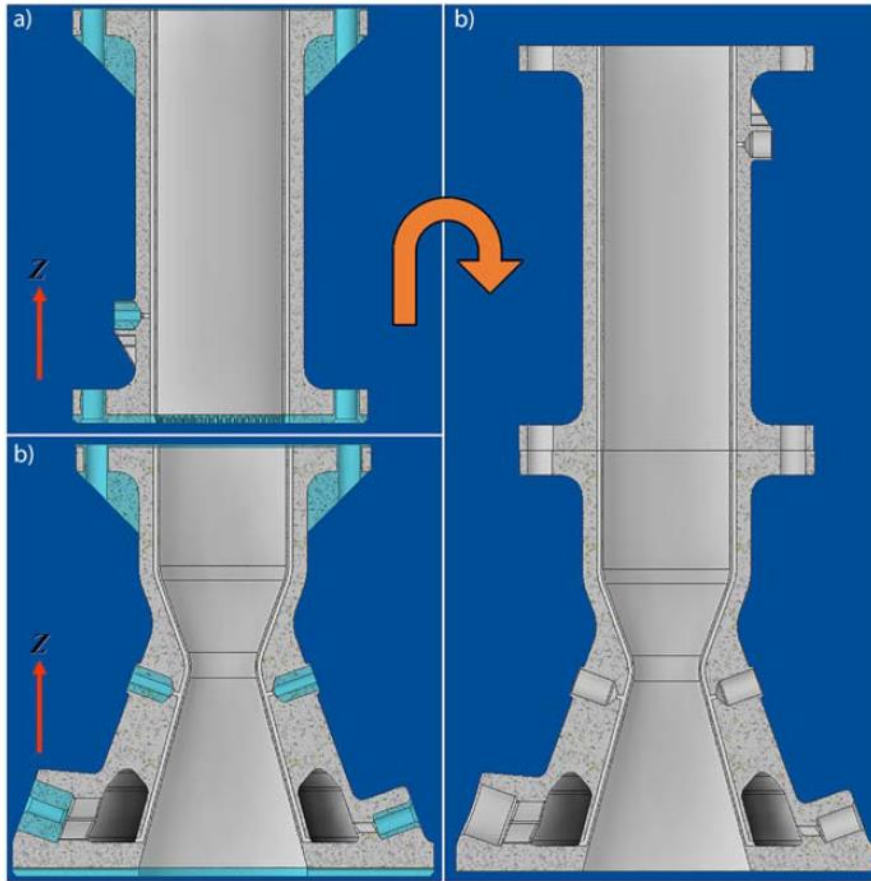


Fig. 7.29 a-b) Each L-PBF part orientation for optimized build. c) Assembly of parts.

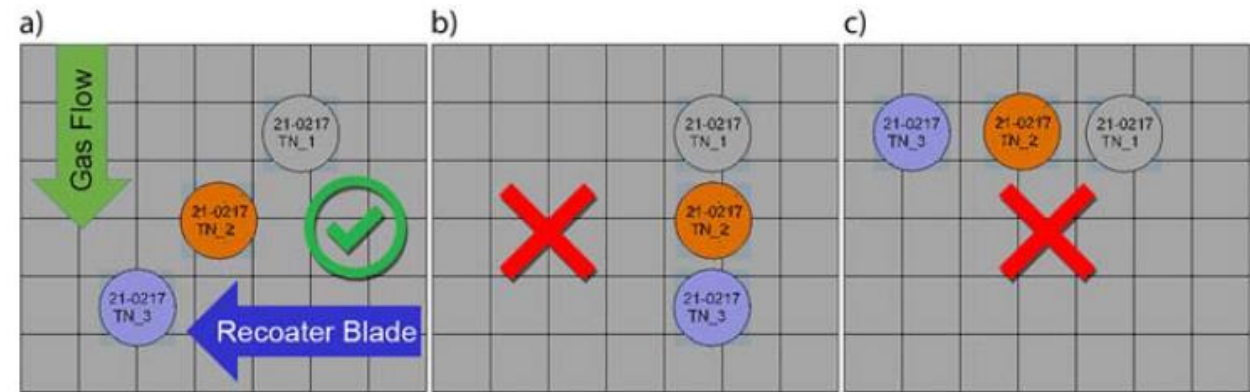


Fig. 7.31 Specimen placement relative to recoater and gas directions.

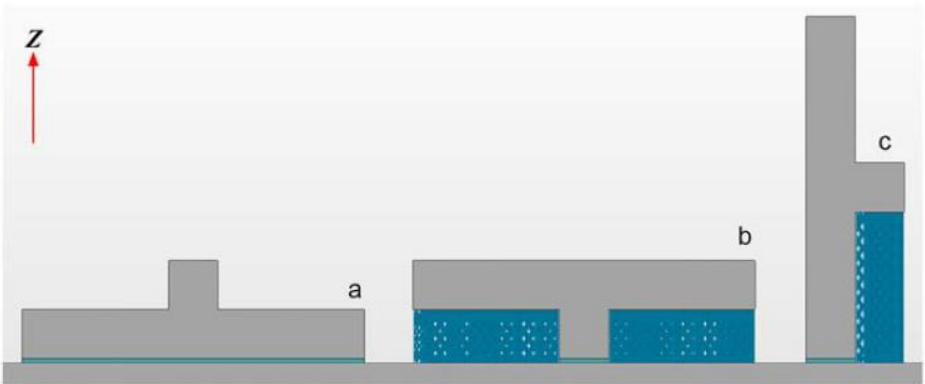


Fig. 7.22 Placement and volume of support structures (blue regions) are highly dependent on part orientation.

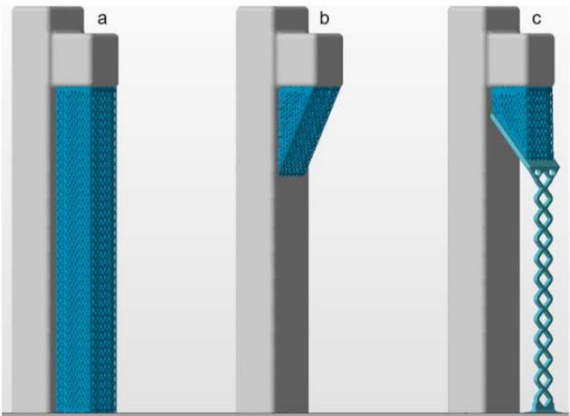


Fig. 7.23 Perforated block supports: a) full length, b) 30° angle, and c) projected onto a user-designed support scaffold.

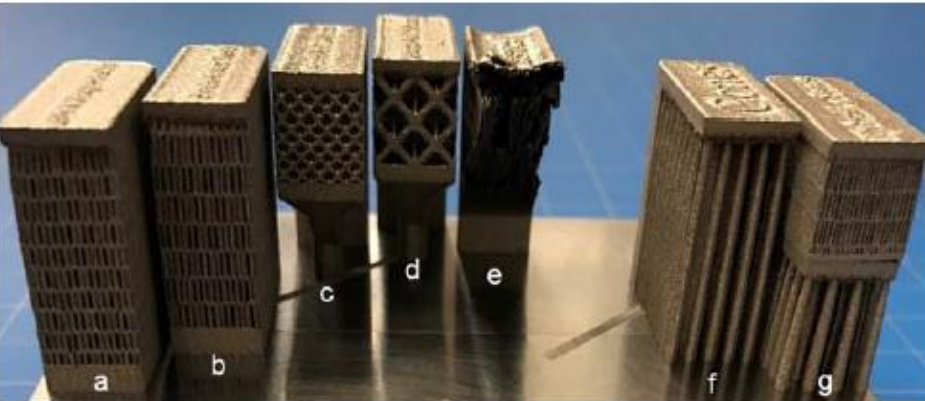


Fig. 5.12 L-PBF support examples. (Source: NASA.)



Fig. 5.13 Manual support removal using hand tools. (Source: NASA.)

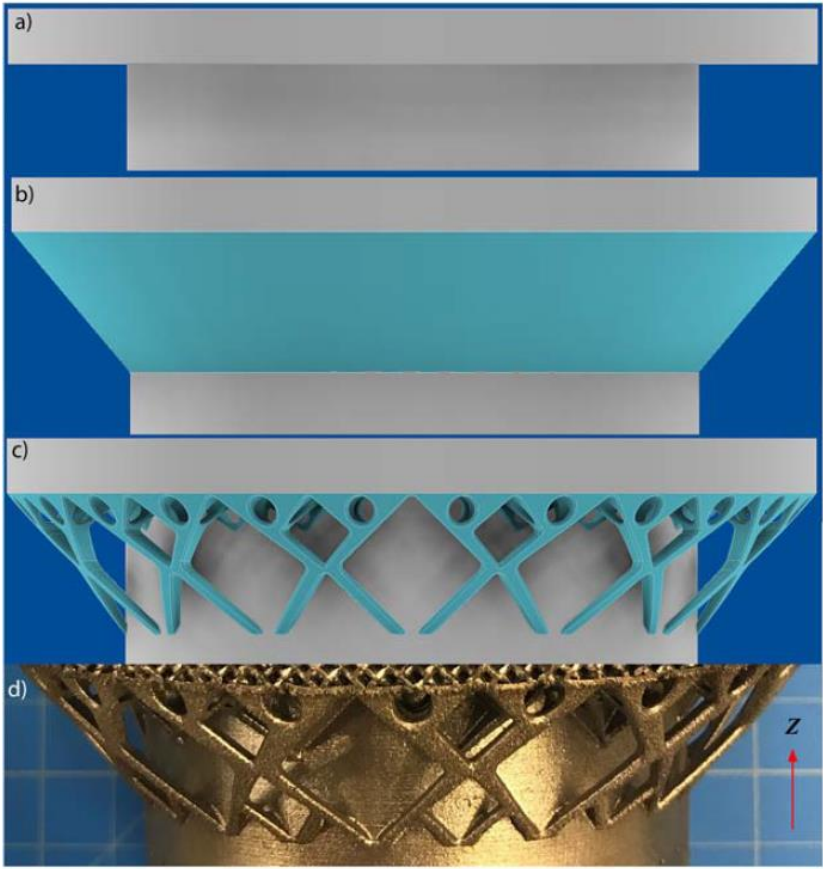


Fig. 7.25 Comparison of a) unsupported overhang flange, b) 40° sacrificial support, c) crown support, and d) Inconel 718 crown support made by L-PBF.

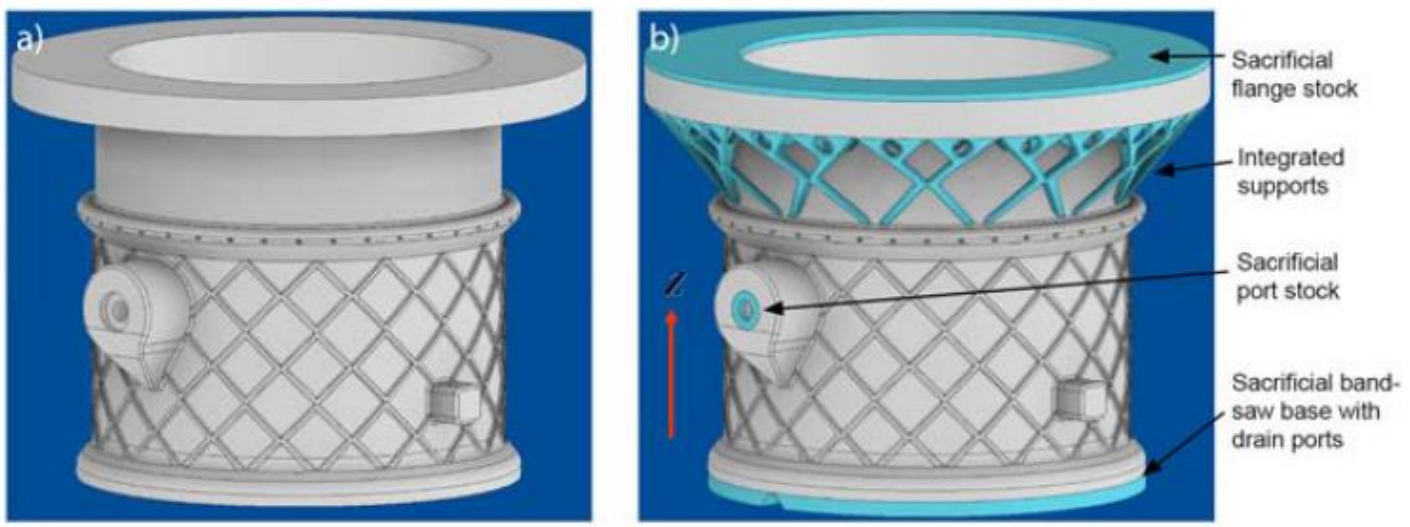


Fig. 7.28 Part a) in final machined condition and b) integrated supports, stock added to interfaces, and drain ports.

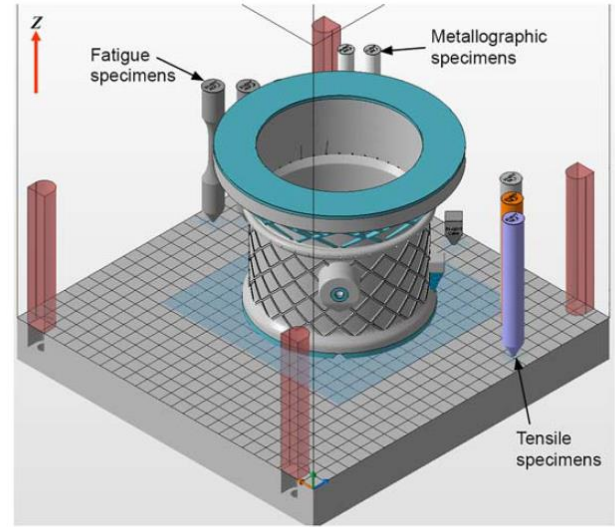


Fig. 7.30 Build layout of a part, support structures, and serialized witness specimens.

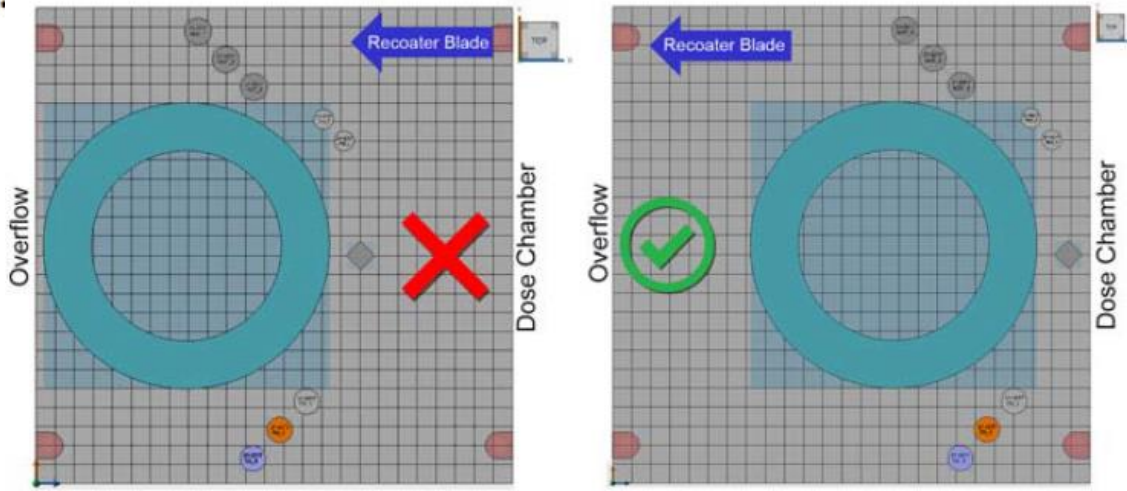


Fig. 7.32 Component placement relative to the dose chamber and recoater blade path.

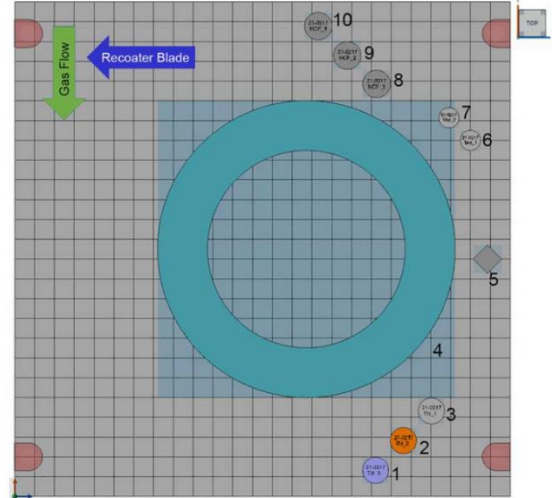
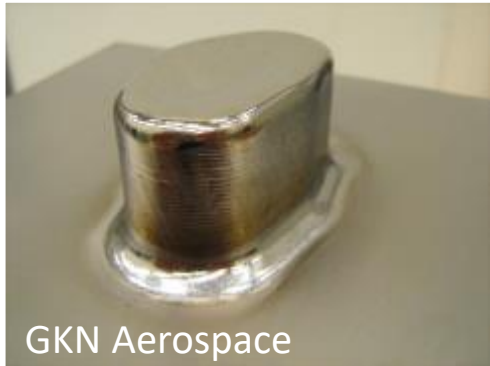


Fig. 7.33 Build layout top view with part positions and scan order optimized for a machine platform with perpendicular gas flow and recoater blade.

Huge Variety of Geometries



GKN Aerospace



DM3D/NASA



DM3D/NASA



RPMI



RPMI/NASA

Substrate

- Size, Material, Temper
- Integral or Sacrificial?

Material

- Chemistry and form
- Material feedstock effect on surface finish

Deposition Strategy and Parameters

- Melt pool size and bead width/height
- Motion platform degrees of freedom and self-supporting angles
- Start / Stop / Transition locations and impact on properties

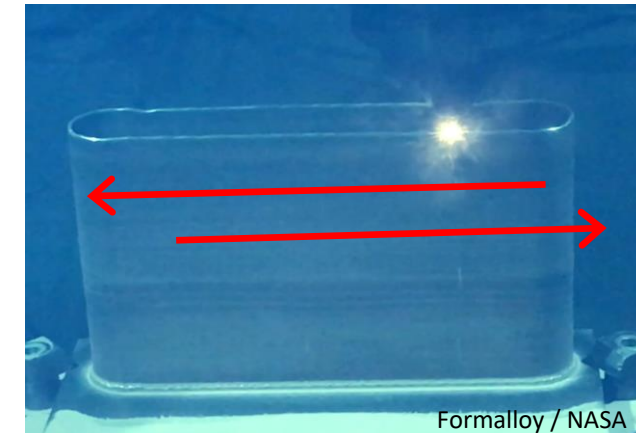
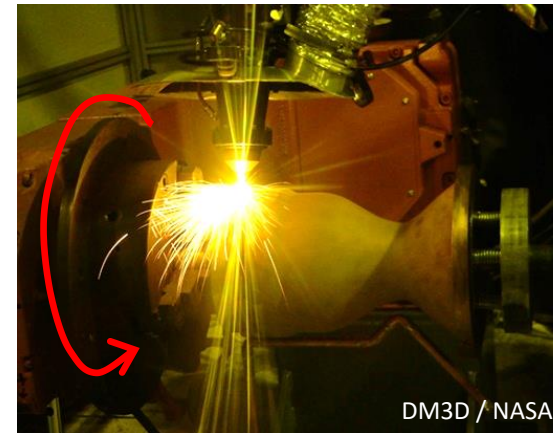
Machining

- Fixturing and datum locations

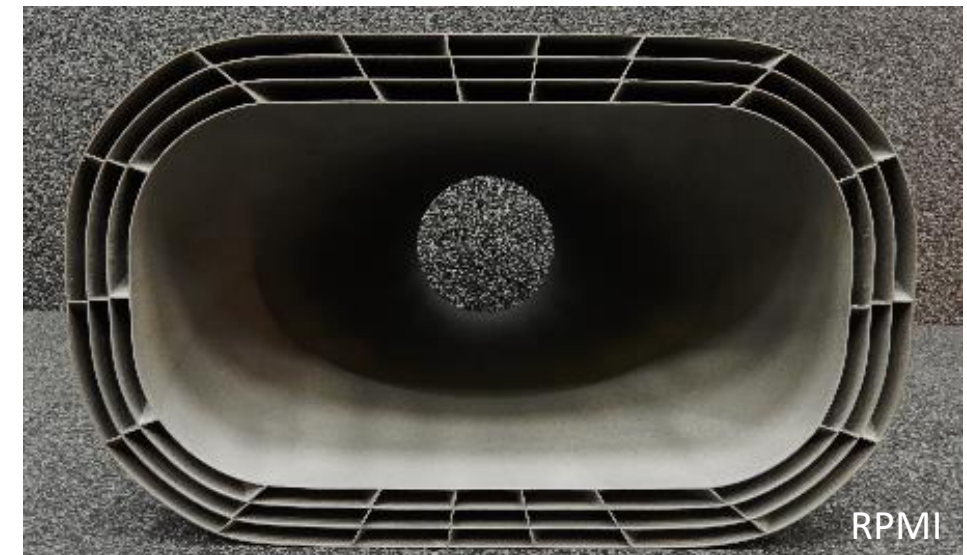
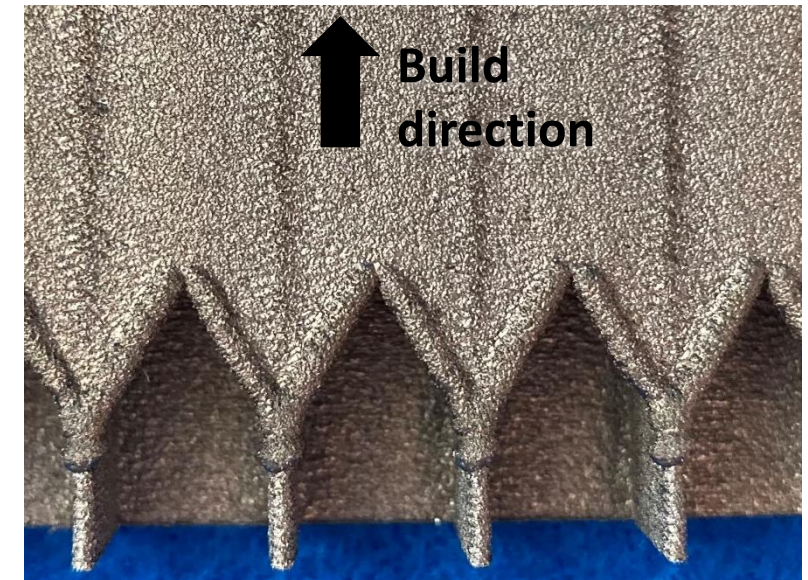
Inspection

- Surface interface with NDE and/or geometry compatibility

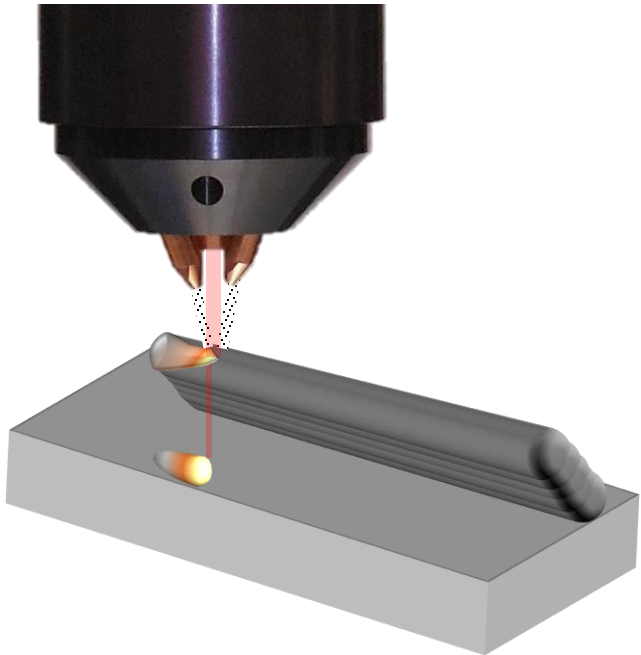
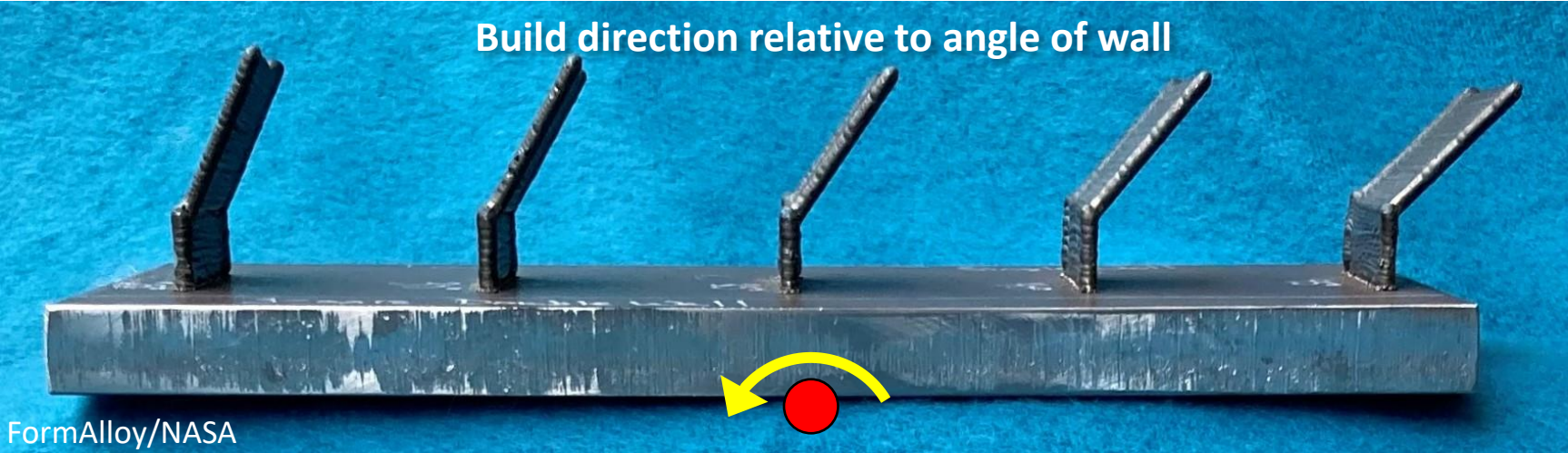
Example: Deposition Strategies



- Wall thicknesses of 1 mm are easily accomplished with LP-DED and LW-DED
- Thinner walls possible, but build angles severely limited and deposition rate reduces significantly
- Internal and complex features are feasible, but within build angle confines
 - Build angles are dependent on the build strategy – continuous motion; 3-axis, other
 - All features in 3D space must be considered including intersecting compound angles
- “Solid” support structures are used – small lattices not possible



Build Angles depend on strategy



*Image courtesy of RPMI

Ability to use multiple axes for complex features fabricated locally



RS25 Powerhead demonstrator using LP-DED under NASA SLS Artemis Program (NASA/RPMI)

Deposition Rate and Geometry

Laser Power: 1070 W	Laser Power: 2000 W	Laser Power: 2620 W
Dep. Rate: 1 in ³ /hr (23 cc/hr)	Dep. Rate: 3 in ³ /hr (49 cc/hr)	Dep. Rate: 5 in ³ /hr (82 cc/hr)
Deposition Time: 24 hours	Deposition Time: 11 hours	Deposition Time: 6 hours



Courtesy: RPM Innovations



Post-Processing

General Process Flow (Post-Processing)

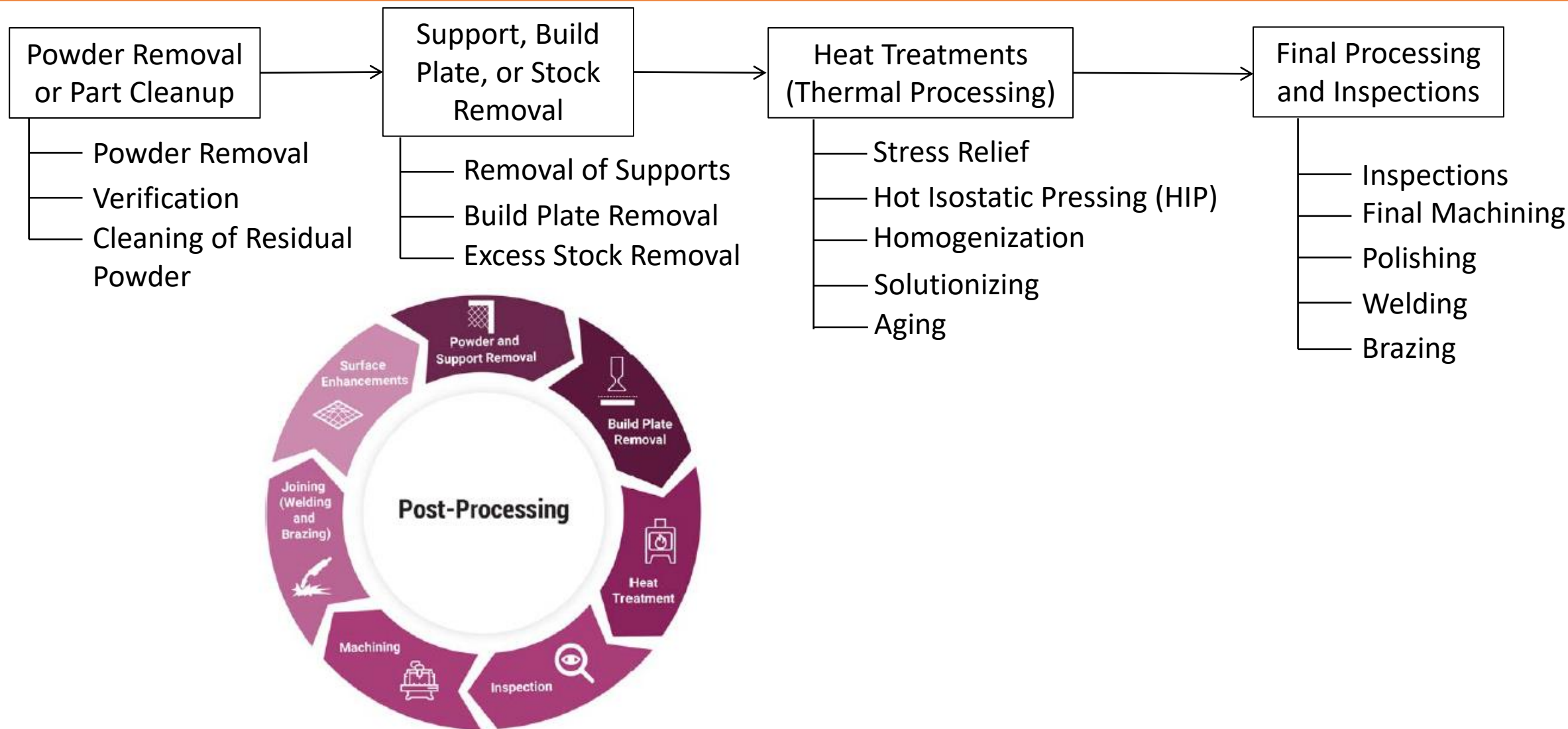


Fig. 5.1 General post-processing steps. The iterative aspect should be considered during the design phase.

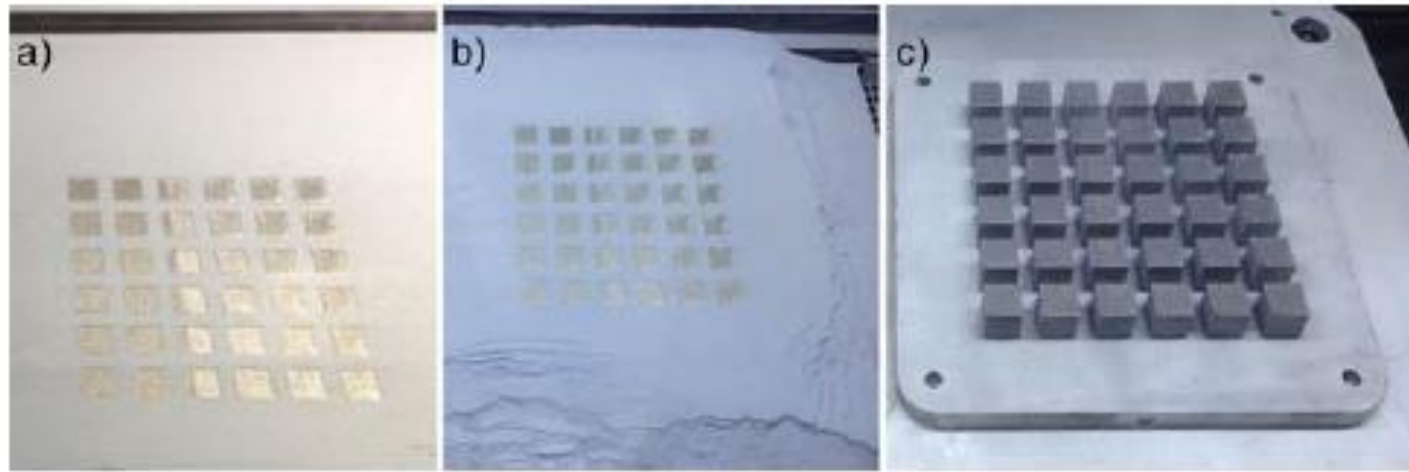


Fig. 5.3 Unpacking example: a) Build completion. b) Build plate raised. c) Powder removed.

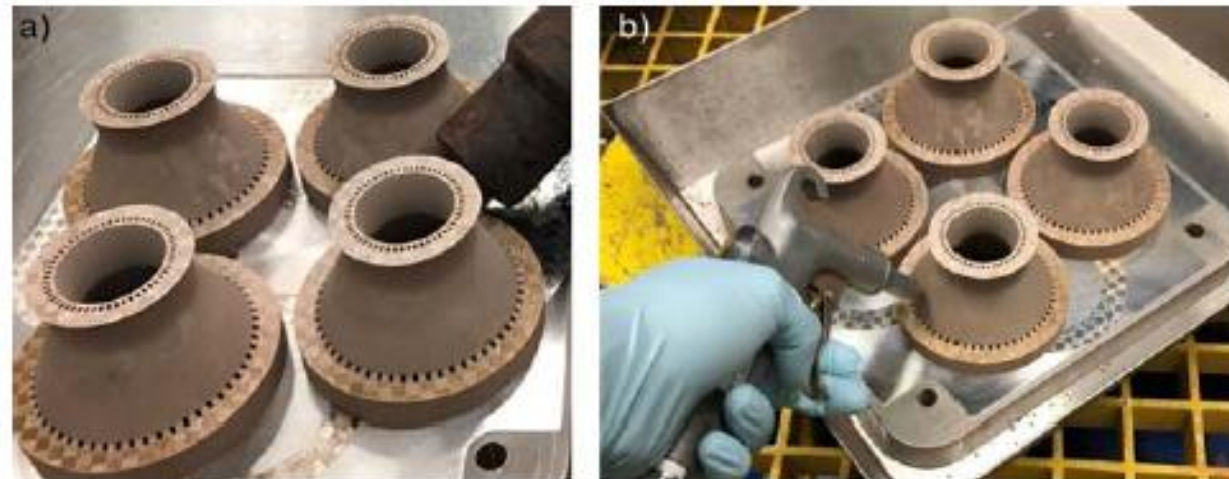


Fig. 5.8 Powder removal with a) a powder vacuum and b) compressed air. (Source: NASA.)

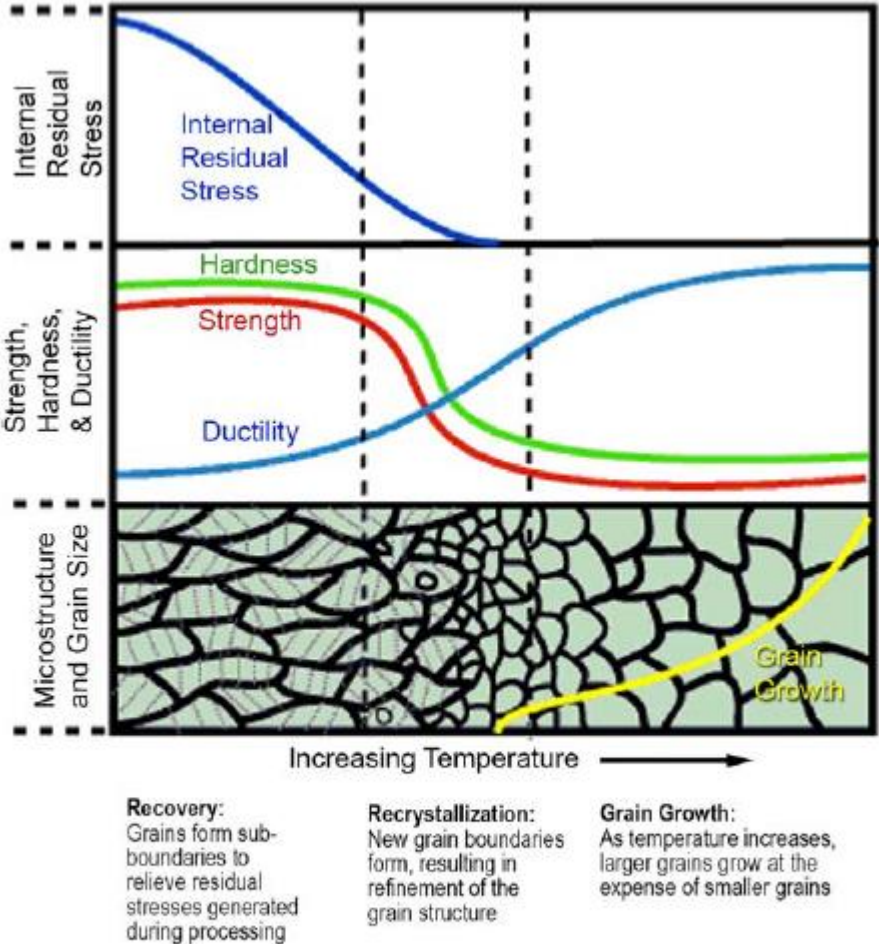


Fig. 4.20 Effects on metal alloy properties of the temperature-dependent recovery, recrystallization, and grain growth regions. (From GATE Metallurgical Engineering [58]; reprinted with permission of GATE Metallurgical Engineering.)

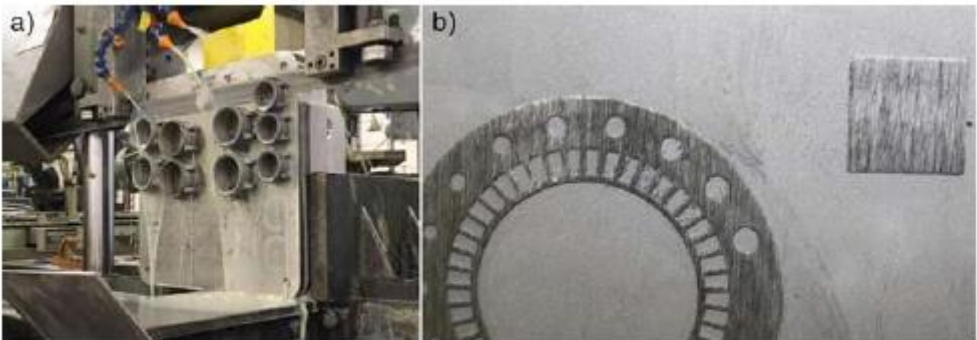


Fig. 5.22 a) Band saw cutting parts from build plate. b) Build plate surface after parts removed.



Fig. 5.23 L-PBF aluminum part fixtured wire-EDM cut chamber before the removal of specimens. (Source: Quadrus Advanced Manufacturing.)

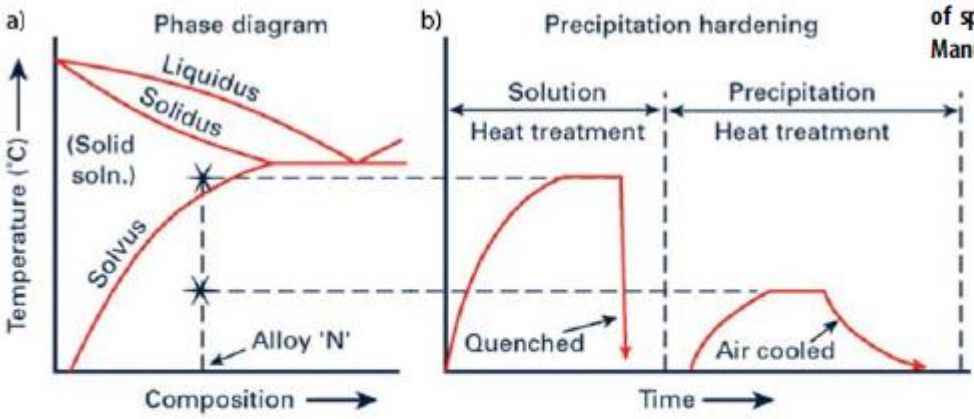


Fig. 4.22 a) General phase diagram and b) corresponding heat-treatment schedule for precipitation hardening. (From Ogunsanya et al. [67]; reprinted under the Creative Commons Attribution-Noncommercial 3.0 Unported License [CC BY-NC 3.0] license, <https://creativecommons.org/licenses/by-nc/3.0/>.)

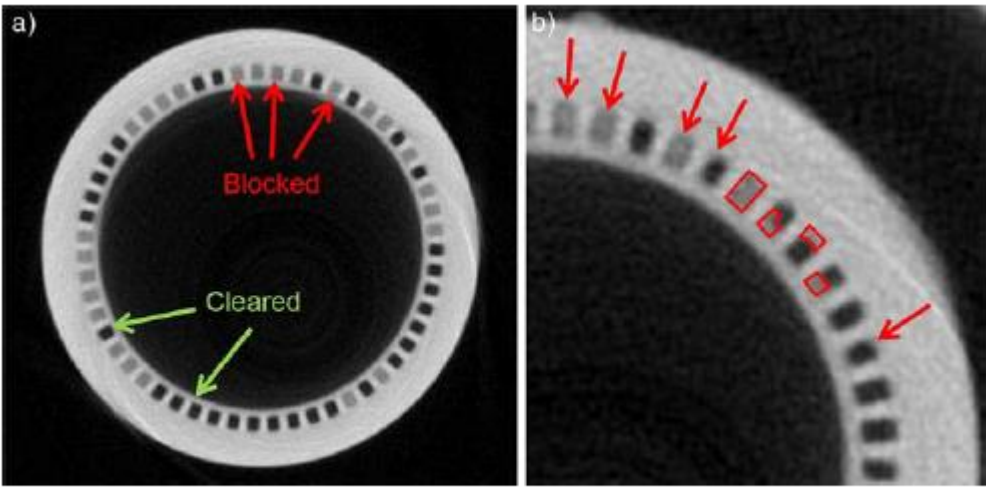


Fig. 5.11 X-ray images of a GRCop-84 chamber with trapped powder in channels. (Source: NASA.)

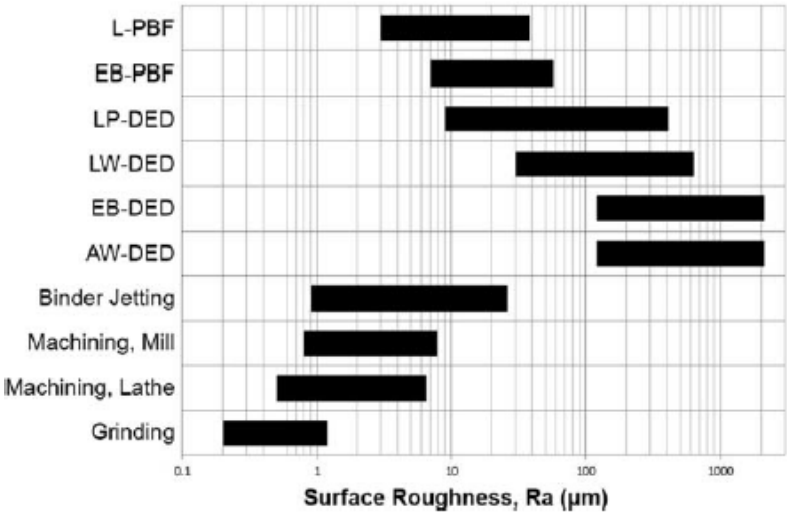


Fig. 5.50 General surface roughness values for selected metal AM processes.



Fig. 5.20 Different chemical support removal methods for original unaltered supports from the L-PBF process. (Source: NASA.)



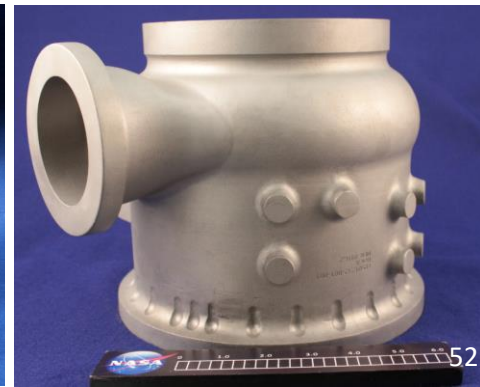
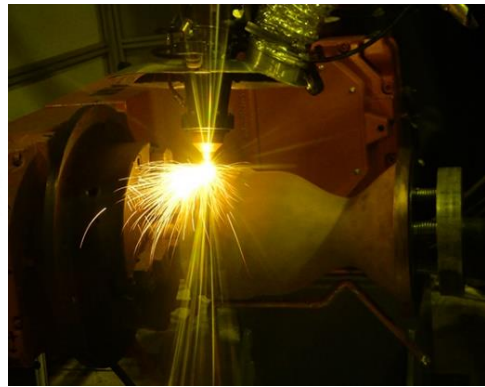
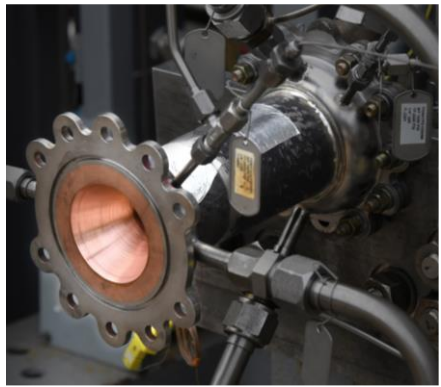
Post-Processing Summary



	Powder Removal and Verification	Support Removal*	Stress Relief**	Build Plate Removal	Heat Treatment Required?	Post-Curing	Final Machining ***
Laser Powder Bed Fusion (L-PBF)	Y	Y	Y	Y	Y	N	O
Electron Beam Powder Bed Fusion (EB-PBF)	Y	Y	N	Y	Y	N	O
Blown Powder Directed Energy Deposition (BP-DED)	Y	Y	Y	Y	Y	N	Y
Arc-Deposition DED	N	N	Y	Y	Y	N	Y
Laser Hot-wire DED	N	N	Y	Y	Y	N	Y
Electron Beam DED	N	N	Y	Y	Y	N	Y
Laser Wire DED	N	N	Y	Y	Y	N	Y
Ultrasonic	N	N	N	N	O	N	Y
Friction Stir	N	N	N	N	O	N	Y
Coldspray	N	N	N	Y	O	N	Y
Binder Jet	Y	O	N	N	Y	Y	O

Y = Requires operation
N = Does not require
O = May Require

- Various AM processes have matured for rocket propulsion applications each with unique advantages and disadvantages.
- AM is not a solve-all; consider trading with other manufacturing technologies and use only when it makes sense.
- **Complete understanding of the design process, build-process, feedstock, and post-processing is critical to take full advantage of AM.**
- Additive manufacturing takes practice!
- Standards and certification of the AM processes are in-work.
- AM is evolving and imagination is the limit.



Examples

A simple printing exercise can demonstrate the typical workflow

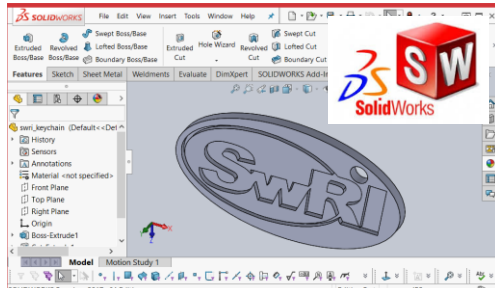
Your widget will change the world.....how can you print it?



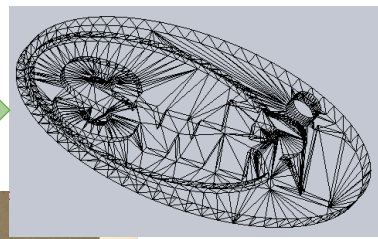
Progression from your design to the machine



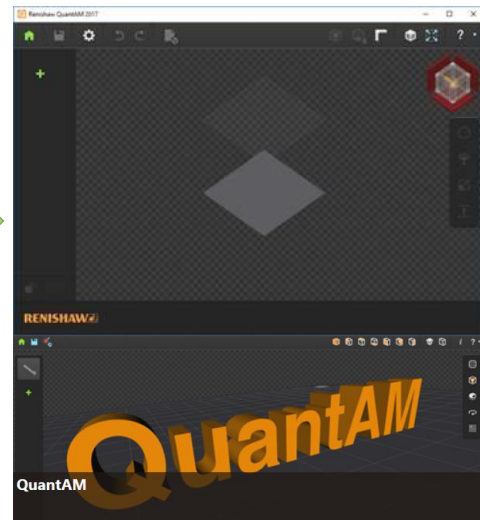
Create
CAD



Generate
STL



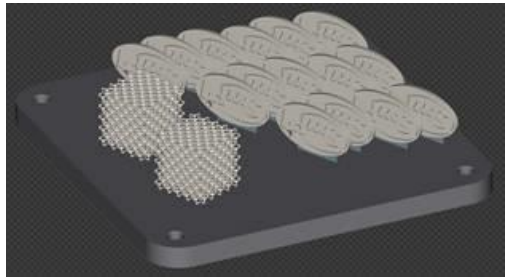
Build
Software



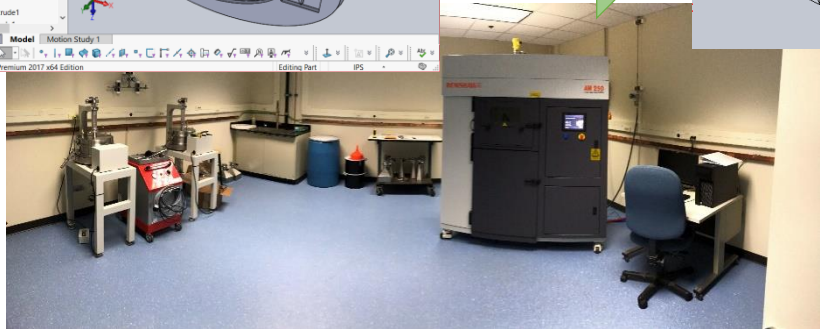
Create Single Part
Layout



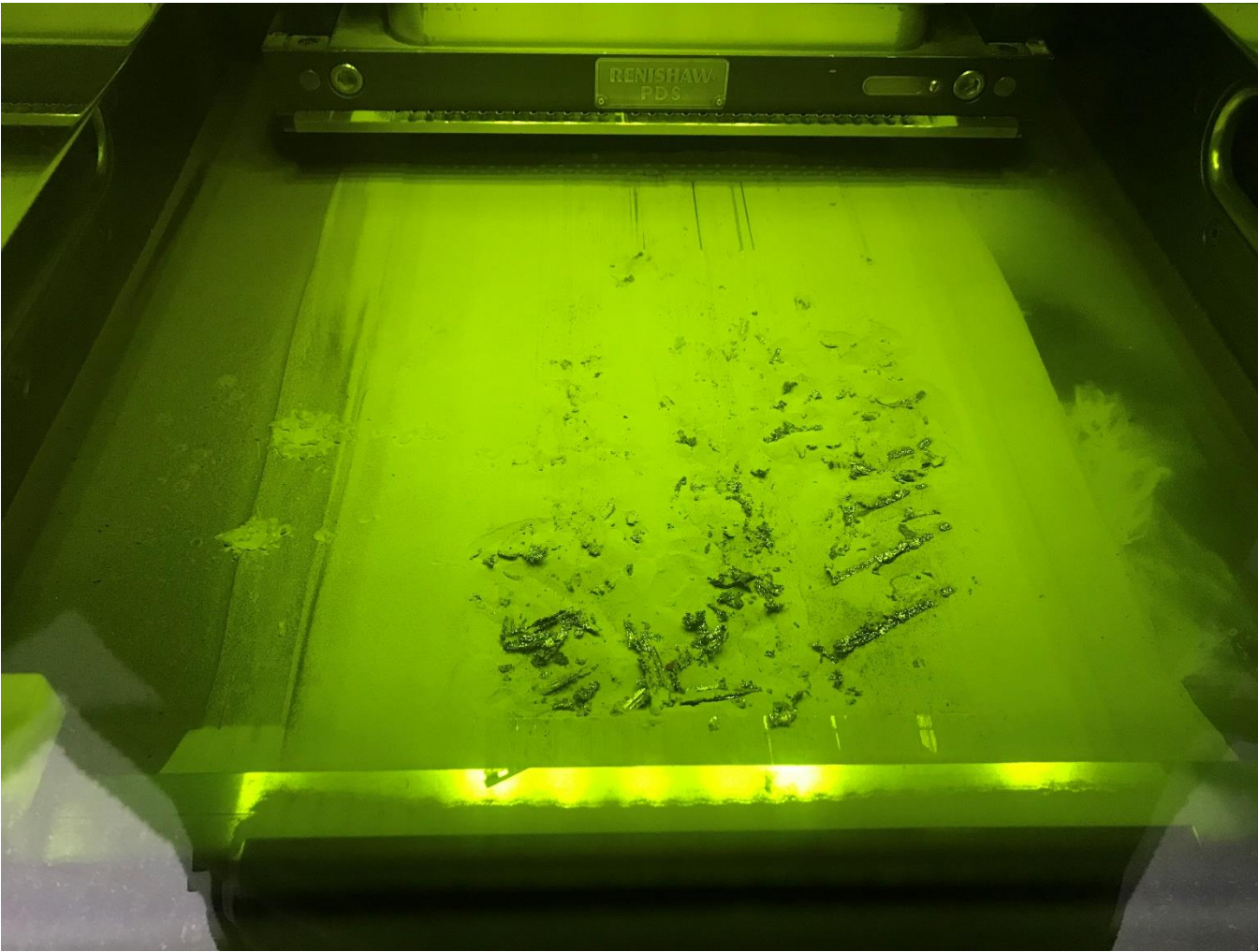
Create Build
Layout



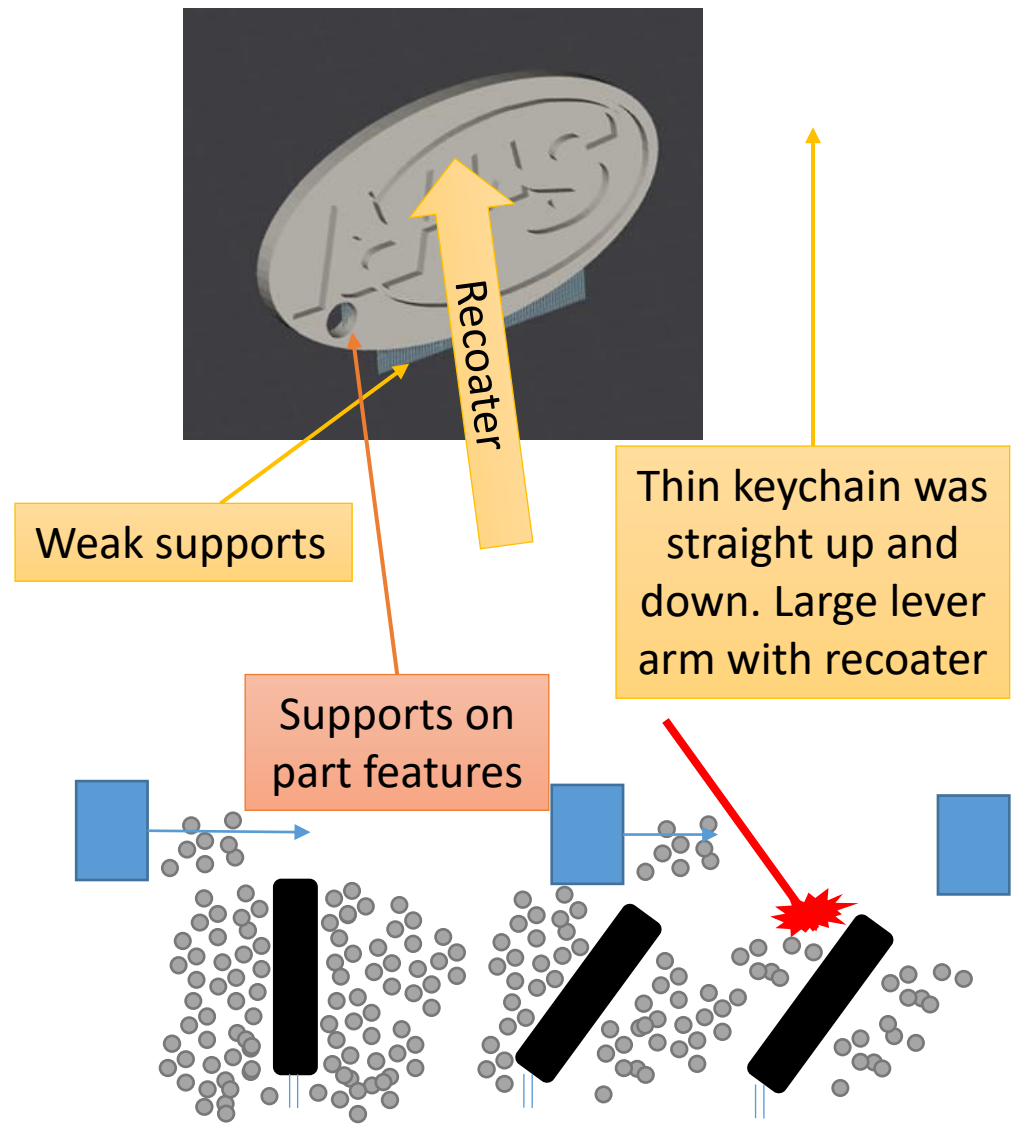
Off to the
Machine!



Unexpected results should be expected



What happened?!?!



Taking your time and thinking ahead can save headache

Improvements to build plan

No supports on features

Another Canting Example

Canted with respect to recoater arm

Canted with respect to build plate

Successful build!



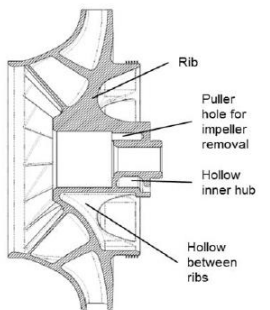
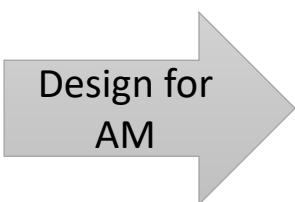


A real AM workflow example: Closed Impeller

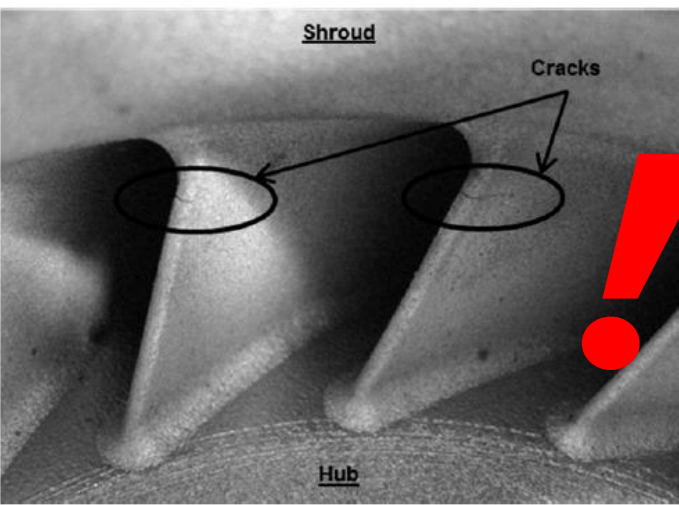
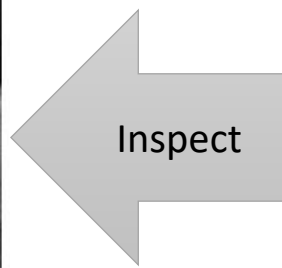
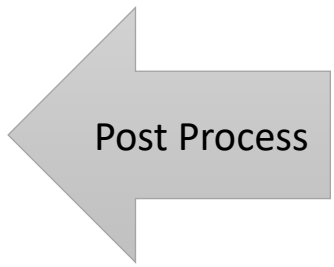
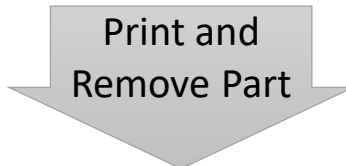
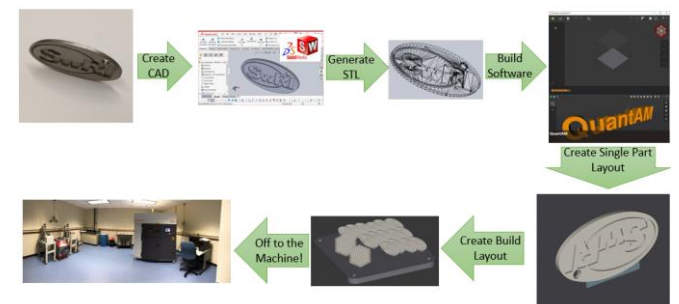
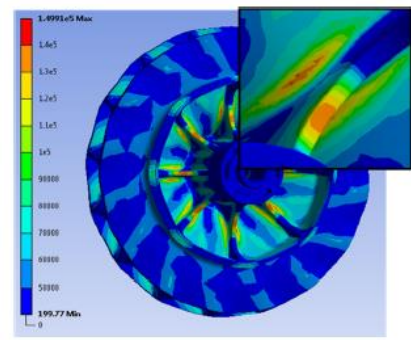




...Almost... A real AM workflow example: Closed Impeller

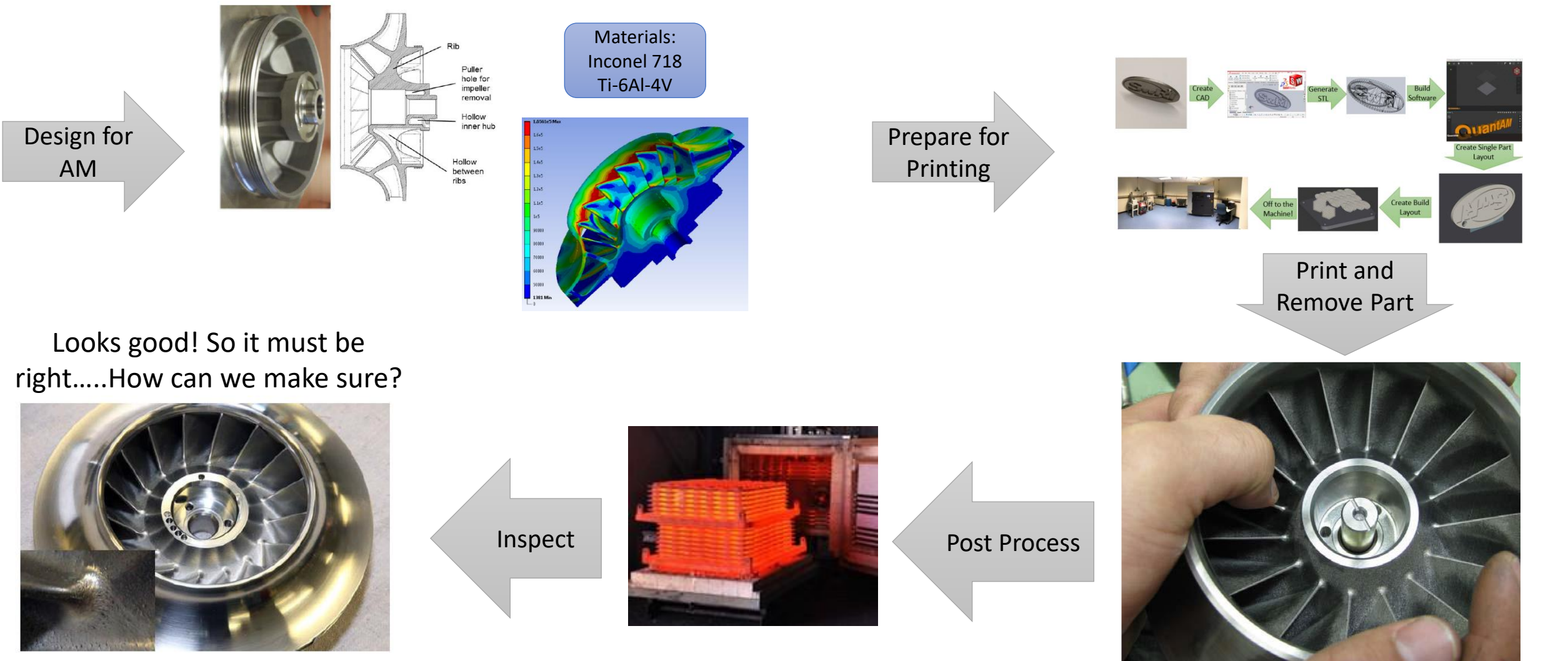


Material:
SS 17-4 PH



What happened?!?!

The component was redesigned using new material and successful prints were taken off the machine



Looks good! So it must be right....How can we make sure?

Non-Destructive Evaluations



Support material remains after extrude hone finish

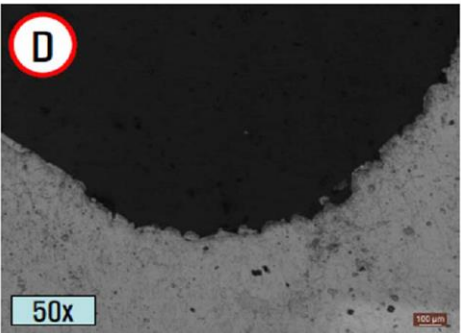


Figure 12. Magnified View of Fillet Region Between Impeller Blade and Shroud

Destructive Evaluation

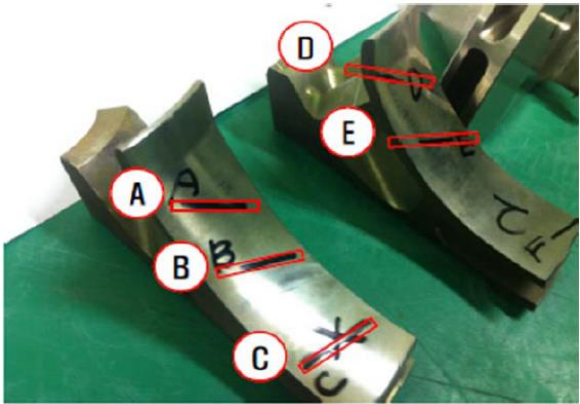


Table 2. Dimensional Accuracy of Manufactured Impellers

Impeller	Impeller Exit Width Accuracy (inches)	Flow Path Surface Roughness (R _a)
1 st Generation 0.08 ϕ Impeller	+0.011	NA
1 st Generation 0.11 ϕ Impeller	NA	NA
2 nd Generation 0.08 ϕ Impeller Variation 'a'	-0.015 to -0.010	63-125
2 nd Generation 0.08 ϕ Impeller Variation 'b'	-0.011 to -0.005	7-32
2 nd Generation 0.08 ϕ Impeller Variation 'c'	-0.005 to +0.000	16
2 nd Generation 0.11 ϕ Impeller Variation 'a'	-0.014 to -0.012	63-125
2 nd Generation 0.11 ϕ Impeller Variation 'b'	-0.005	63-125
2 nd Generation 0.11 ϕ Impeller Variation 'c'	-0.003	16-92

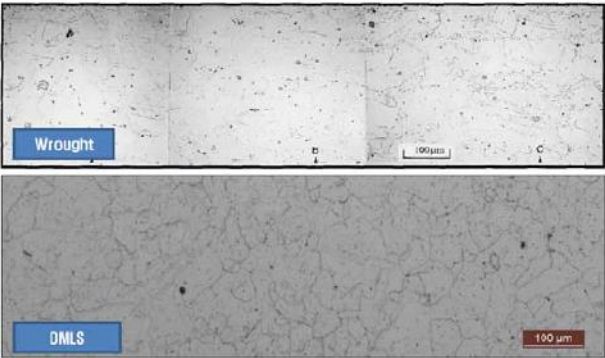


Figure 13. Comparison of Grain Size Between Wrought Inconel 718 and DMLS Inconel 718

Allison et. al. "Manufacturing and Testing Experience with Direct Metal Laser Sintering for Closed Centrifugal Compressor Impellers", 2014

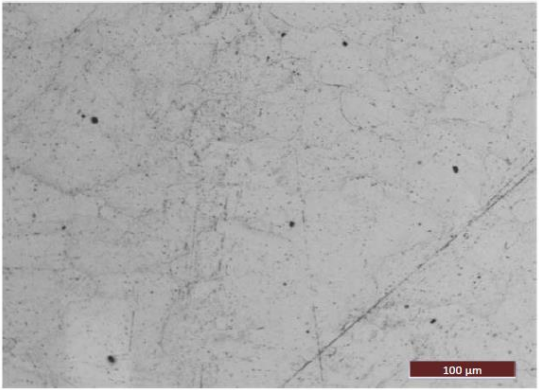


Figure 14. Magnification of DMLS Inconel 718 Sample Showing Micro-Porosity

Application Testing

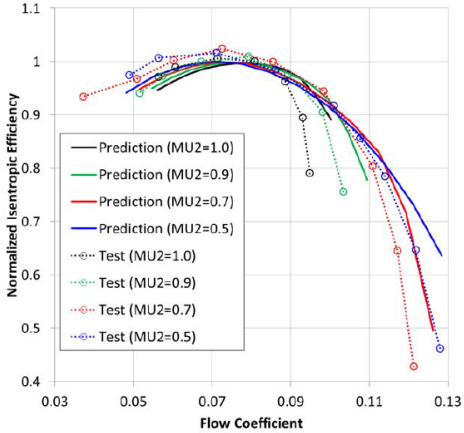


Figure 18. Comparison of Predicted and Tested Normalized Isentropic Efficiency vs. Flow Coefficient

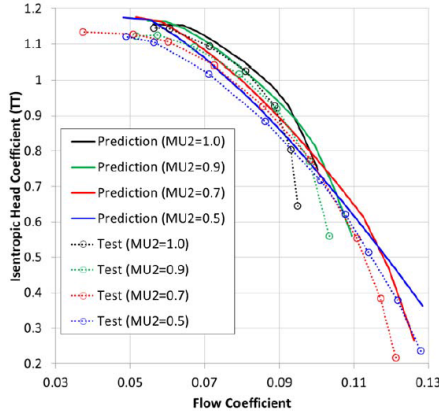


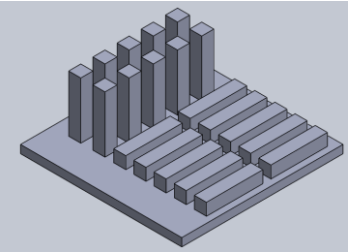
Figure 17. Comparison of Predicted and Tested Head vs. Flow Coefficient



Mechanical property characterization of printed IN738 were measured for high-temperature applications



Specimens



Historical Cast In738 Data

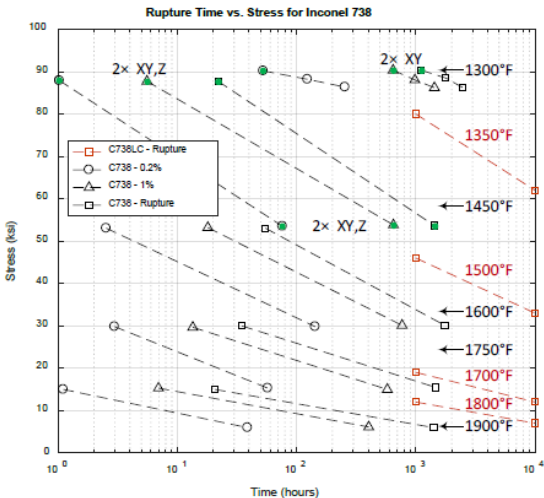
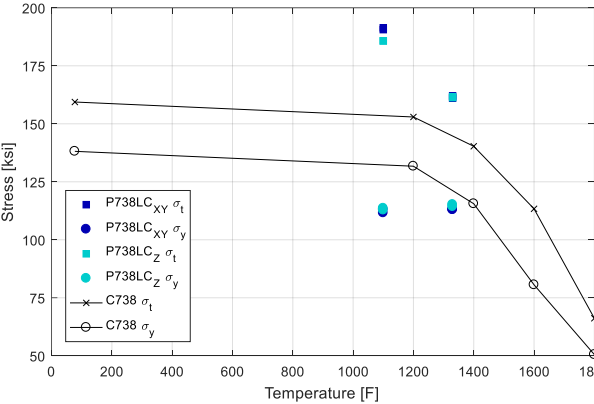
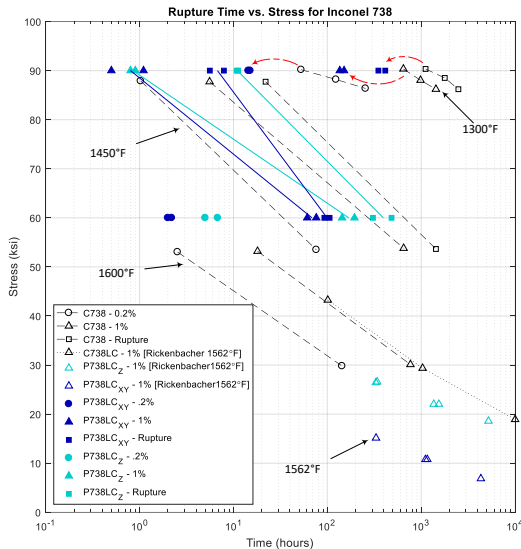


Figure 2: Cast Inconel 738 Creep Sample Data and Associated Test Points (Denoted by Green Accent), Heat Treat - 2050F, 2 hrs, AC +1550F, 24 hrs, AC (data taken from [8])

Printed In738LC Data



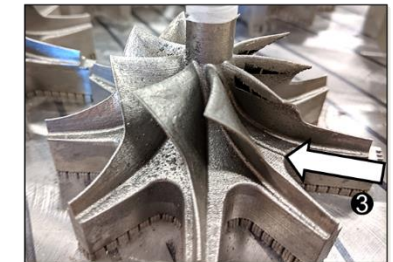
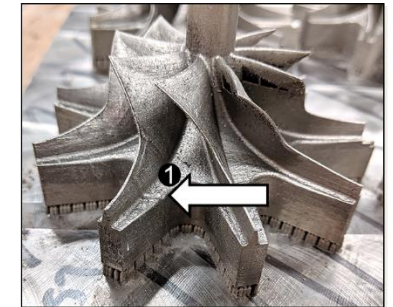
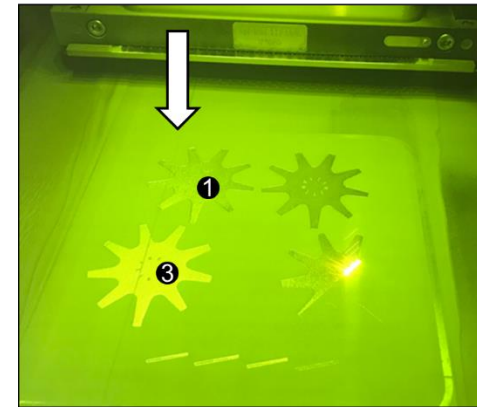
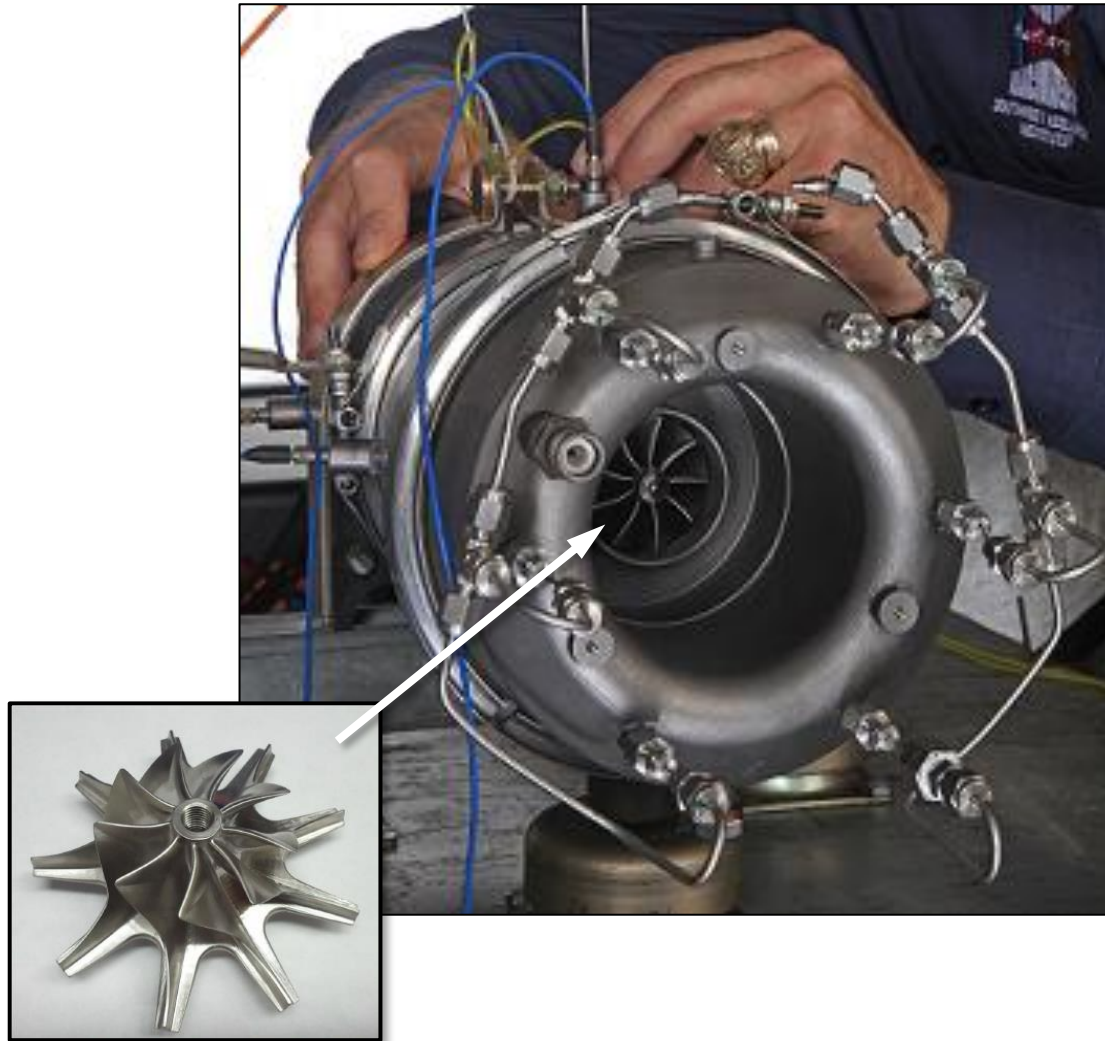
Post Process



Wilkes et. al. "Creep and Tensile Properties of DMLS Printed Inconel 738 Coupons and Comparison to Cast Properties", 2018

Specimen ID	Test Temper	Diameter (Inches)	Ultimate Strength	Yield Strength	Elongation (%)	Reduction Of Area (%)	Fracture Location
S1	1330	0.2507	162,000	113,000	17.5	27.1	Gage
S2	1330	0.2493	161,100	113,000	16.8	23.9	Gage
S3	1100	0.2498	190,600	111,600	15.4	23.5	Gage
S4	1100	0.2496	191,400	113,100	15.6	22	Gage
R1	1330	0.2507	161,300	114,300	21.6	34.1	Gage
R2	1330	0.2507	161,700	115,200	23.4	37.3	Gage
R3	1100	0.2509	185,800	113,600	15.2	23.1	Gage
R4	1100	0.251	185,700	112,800	14.6	22.1	Gage

The AM Process Lifespan





Successful AM application needs access to all the processes

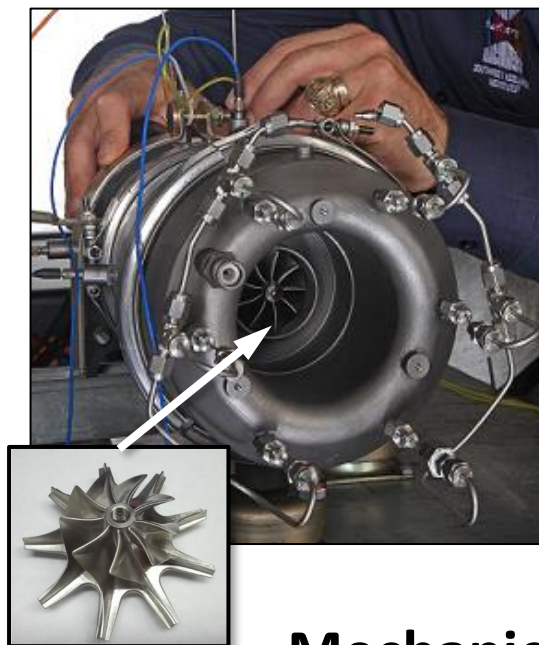
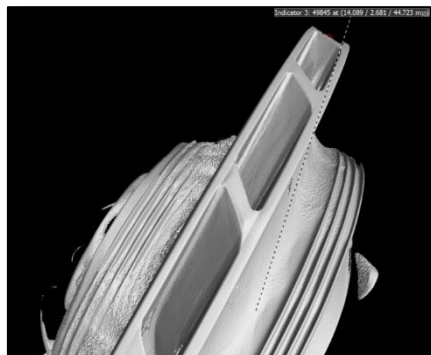
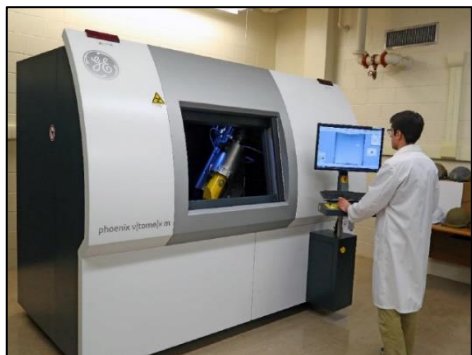


Printing Capability: Renishaw AM250

- 273mm x 273mm build area
- IN 718 capable

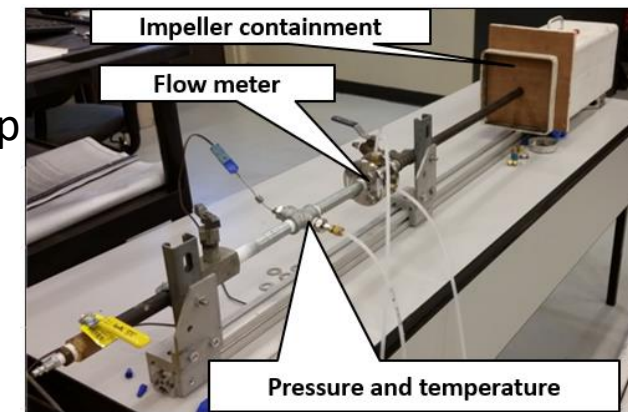
Inspection Capability: CT Scan

- Non-destructive evaluation of impeller



Component Testing: Pressurized Coolant Flow Test Rig

- Shop air (~100 psi)
- Measure pressure drop
- Measure flow rate



Application: 12.5kW Gas Turbine

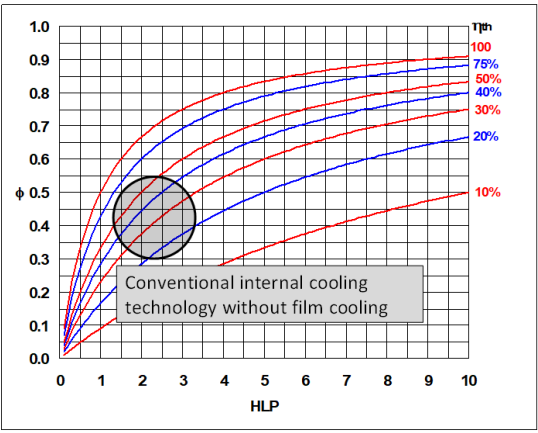
- 118,000 rpm
- Material IN718
- 90mm diameter

Mechanical Testing & Characterization Lab

- Surface characterization
- Destructive evaluation tests



1D heat transfer analysis to determine passage size to achieve 550°C metal temperature using available compressor bleed air

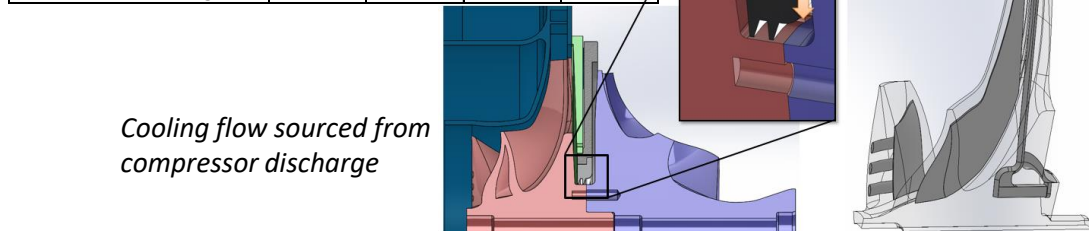


$$\phi_m = \frac{T_g - T_{m,ext}}{T_g - T_{c,in}}$$

$$HLP = \frac{W_c C_p}{h_g A_g} = \frac{T_g - T_{m,ext}}{T_{c,out} - T_{c,in}}$$

The turbine cooling requirements are defined to achieve conventional cooling effectiveness values

	Case 1	Case 2	Case 3	Case 4
Inlet Channel Width [mm]	0.5	0.6	0.75	1
Cooling Split [%]	0.75%	1.08%	1.35%	1.79%
Flow Check [KPa]	-1	40	121	135
Max Mach # [-]	0.92	0.93	0.54	0.37
Tm-ext Max [K]	835	823	823	823
Tm-ext Target [K]	823	823	823	823



Cooling flow sourced from compressor discharge

3D heat transfer and mechanical analysis to determine mechanical integrity and life

118,000 rpm
Fixed axial displacement
Shaft cylindrical support
Assume 550°C-370°C

1202°F Property	Wrought	Printed
Modulus Elasticity	3016.8 ksi	2538.1 ksi
Yield Strength	169.7 ksi	161.0 ksi
Ultimate Strength	204.5 ksi	195.8 ksi

Printed material properties for heat treated IN718 from Strobnier et al. 2015 and Deng et al. 2017

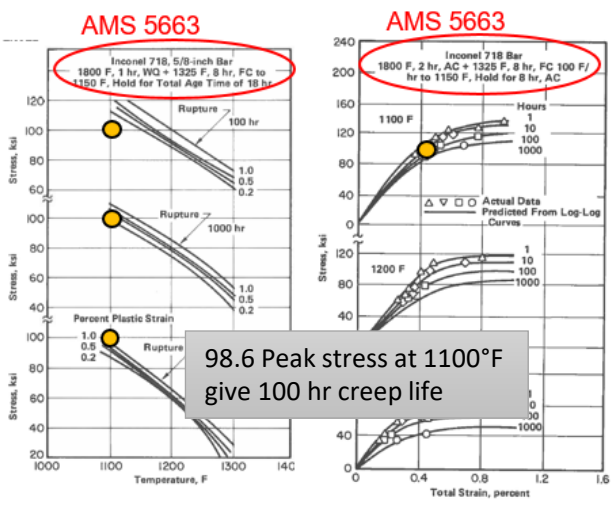
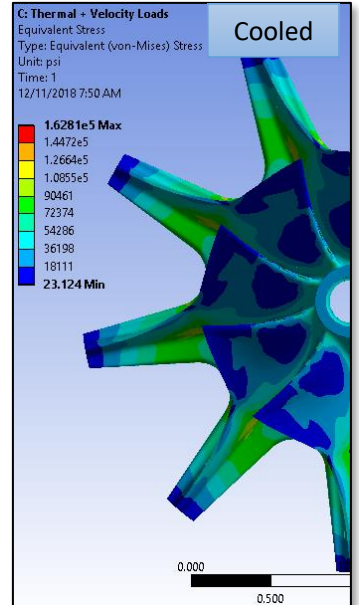
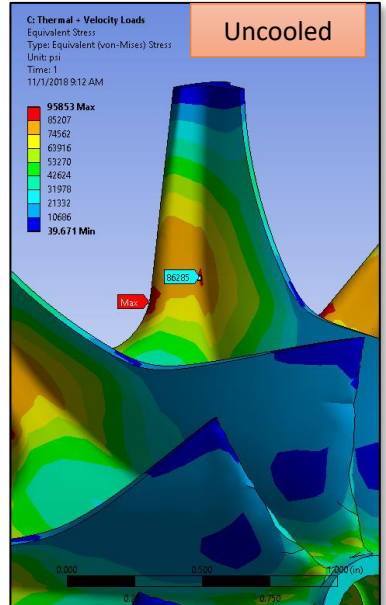
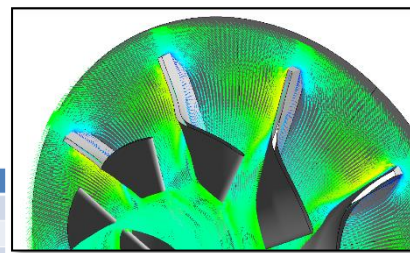


FIGURE 3.041. STRESSES REQUIRED TO CAUSE VARIOUS AMOUNTS OF CREEP AND RUPTURE IN 100, 1000, AND 10,000 HOURS AT TEMPERATURES FROM 1100 TO 1300 F (1)
FIGURE 3.043. ISOCHRONOUS STRESS-STRAIN CURVES AT 1100, 1200, AND 1300 F FOR TIME RANGE 1 TO 1000 HOURS (40)

Ref: 1996, Aerospace Structural Metals Handbook, Purdue University Center for Information and Numerical Data Analysis and Synthesis.

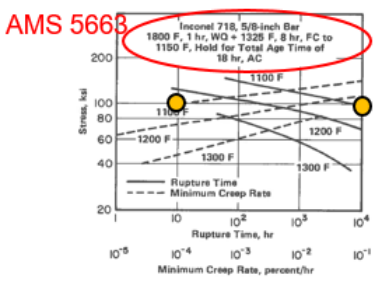
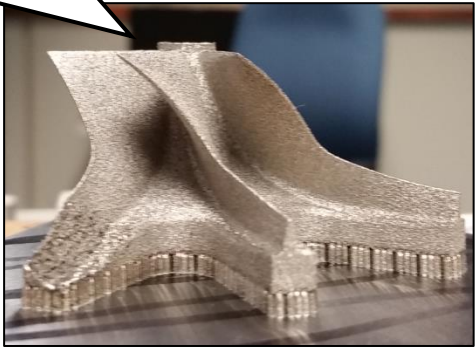


FIGURE 3.042. CREEP RUPTURE TIME AND MINIMUM CREEP RATE OF BAR AS FUNCTIONS OF STRESS IN THE TEMPERATURE RANGE 1100 TO 1300 F (1)


98.6 Peak stress at 1100°F give 100 hr creep life

Several test prints have been completed to determine AM print capabilities and considerations of the design

Quarter geometry for blade angles

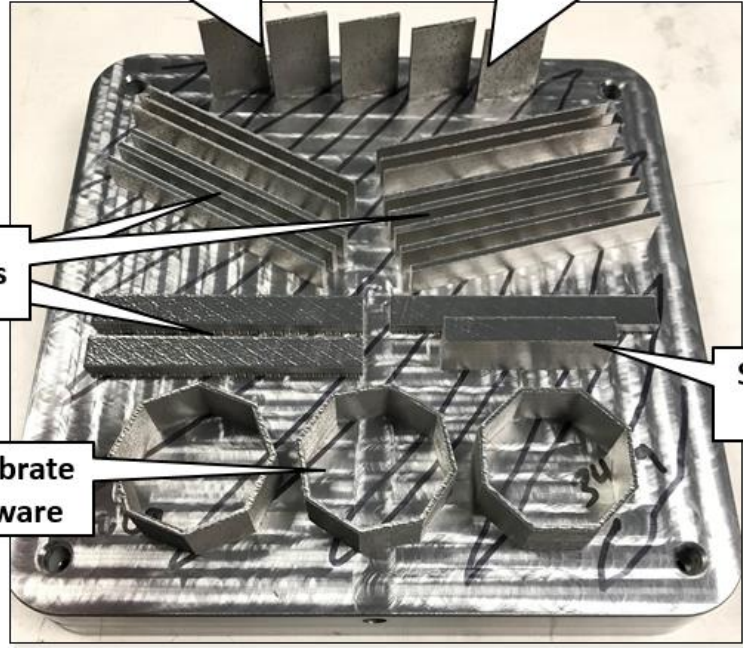


Quarter geometry for cooling channel thickness




Coupons for channel roughness

Coupons for cooling turbulators



What if we account for build distortions?

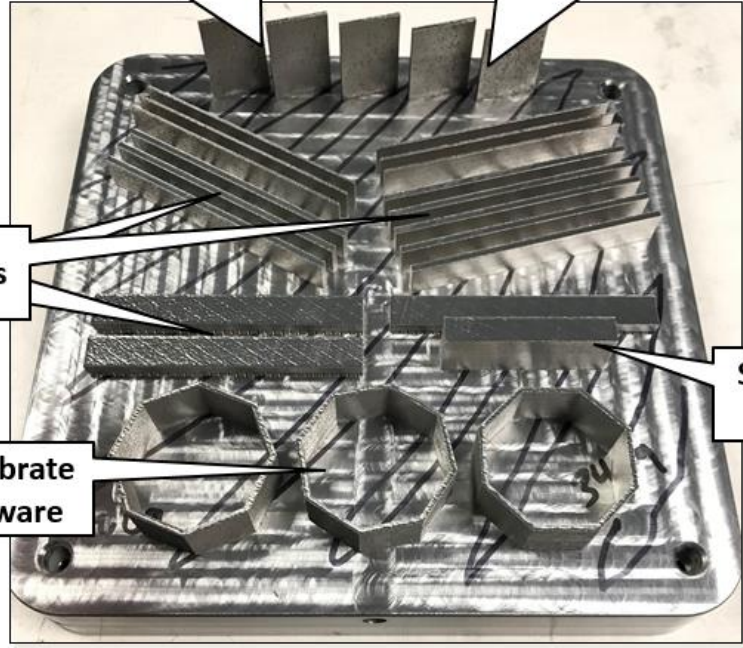
What if we make the blades thicker?



Tensile coupons

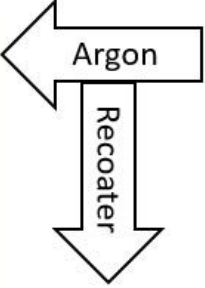
Polygons to calibrate distortion software

Solid block to calibrate distortion software




Argon

Recoater



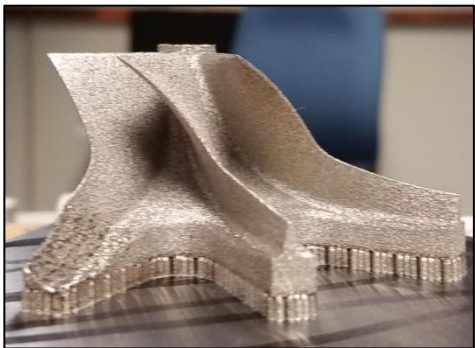
Build CAD geometry using supports (Baseline)

What if we build the impeller directly on the build plate?

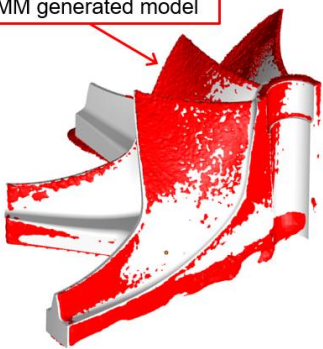


Non-destructive evaluations were used to determine printability of features and expected distortions

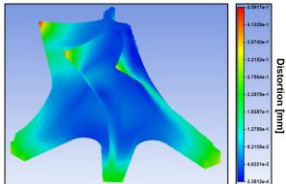
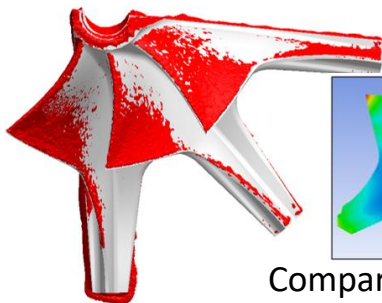
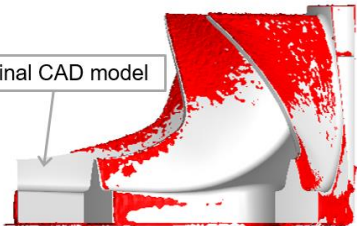
Coordinate Measurement Machine (CMM) inspections show geometric distortions



CMM generated model



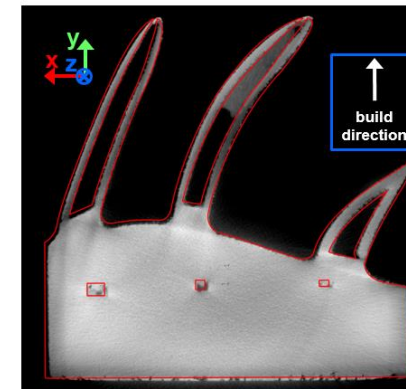
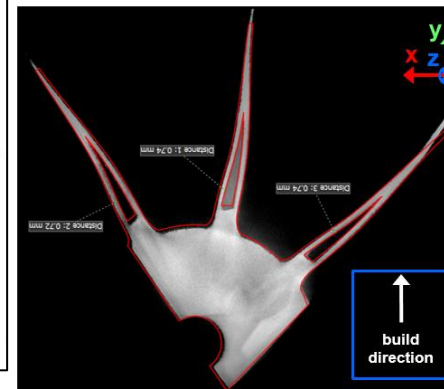
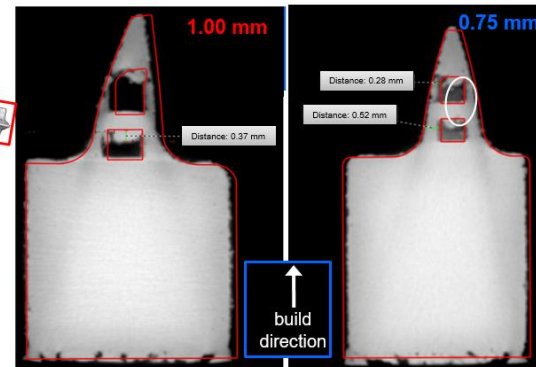
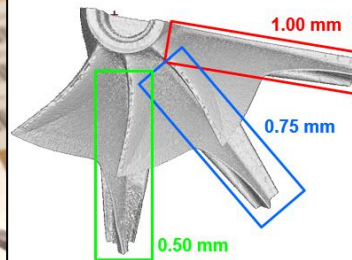
Original CAD model



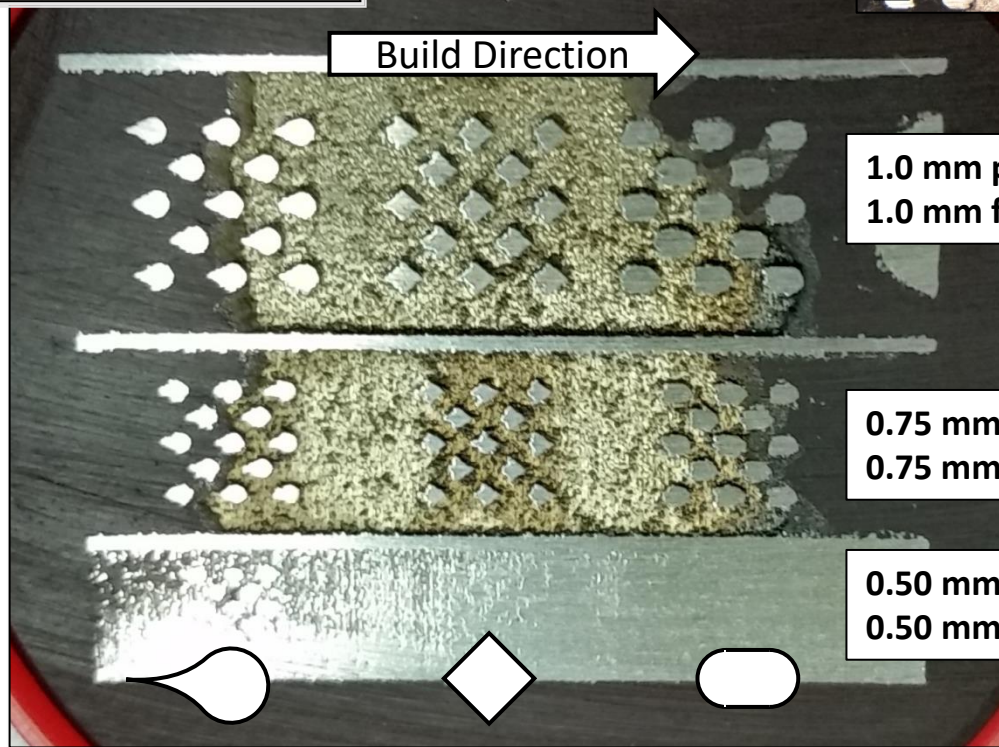
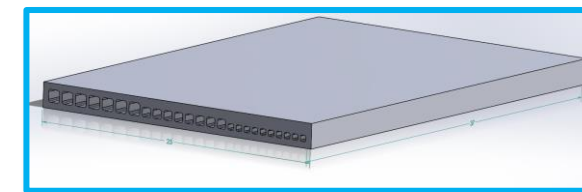
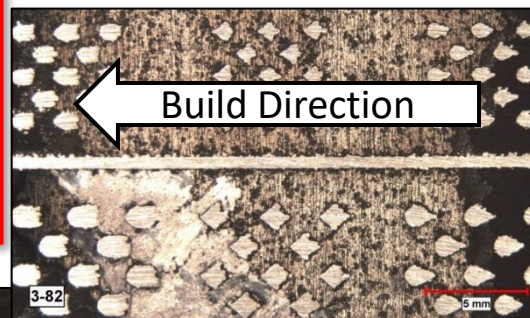
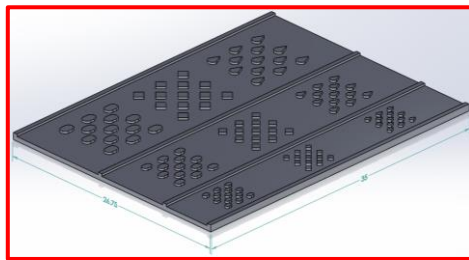
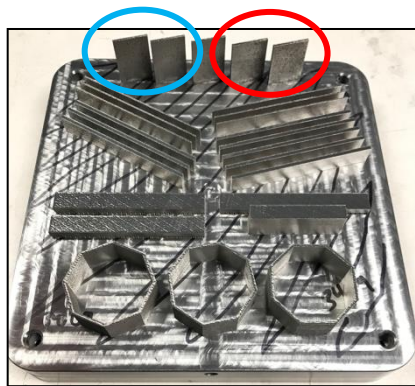
Comparison performed with ANSYS Additive®

Location	Measured Distortion
1	0.51 mm
2	0.43 mm
3	0.31 mm
4	0.39 mm
5	0.24 mm
6	0.34 mm

X-Ray CT Inspections show 0.75 mm cooling channels are repeatable



Teardrop-shaped turbulators had the best build resolution, which is also the most aerodynamic, and 0.75 mm was the minimum repeatable passage width

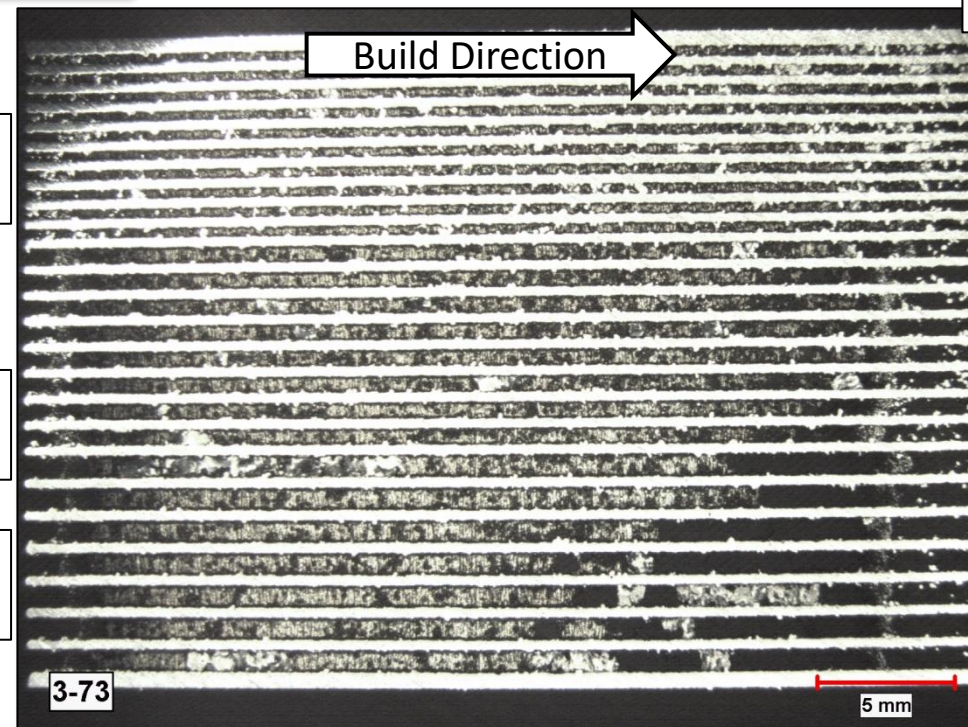


Build Direction

1.0 mm passage height
1.0 mm features

0.75 mm passage height
0.75 mm features

0.50 mm passage height
0.50 mm features



Build Direction

Passage Height:

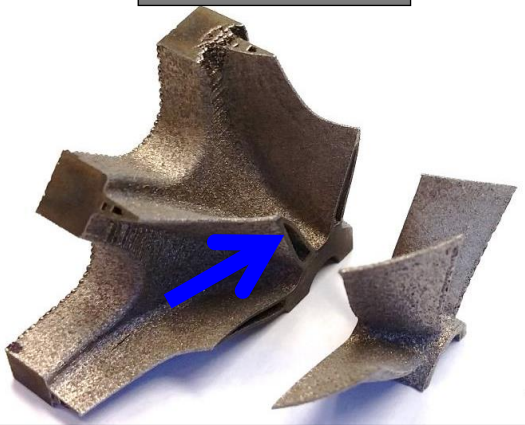
0.50 mm

0.75 mm

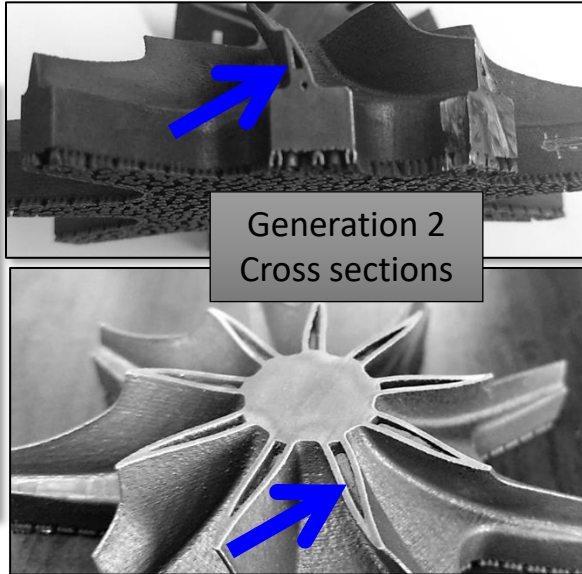
1.0 mm

The cooling passages are modified to allow easy removal of powder prior to stress relief

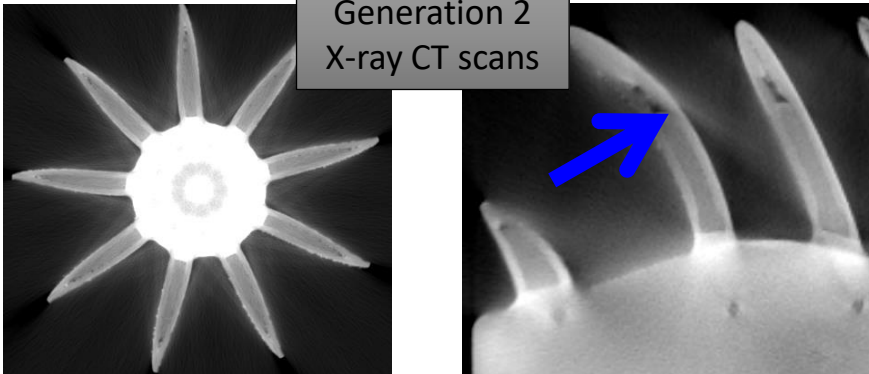
Generation 1
Cross sections



Generation 2
Cross sections



Generation 2
X-ray CT scans

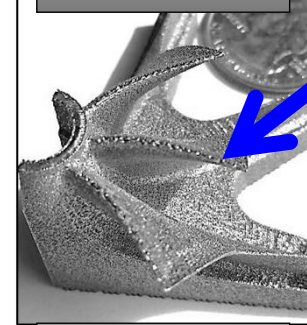


Generation 3 will utilize
vibration apparatus



Vibration & Mechanical Removal
Gradl, P., Mireles, O., and Andrews, N., 2018, "Intro to Additive Manufacturing for Propulsion Systems."

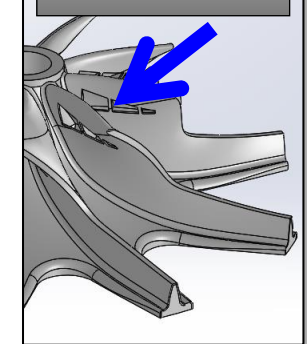
Generation 1



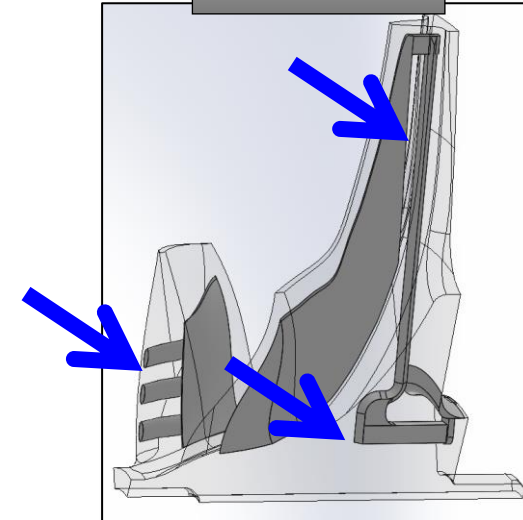
Generation 2



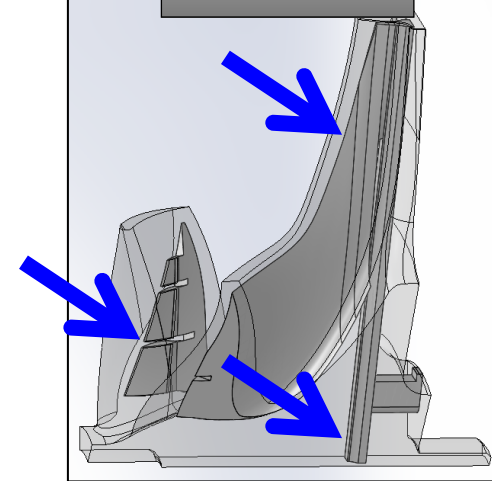
Generation 3



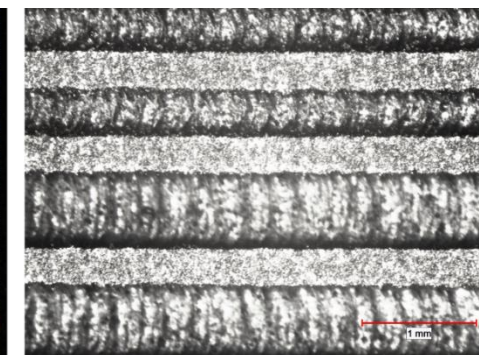
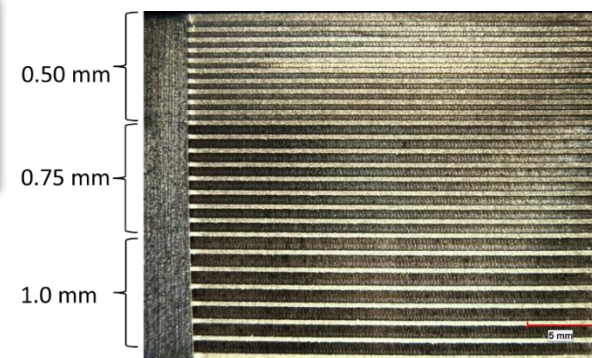
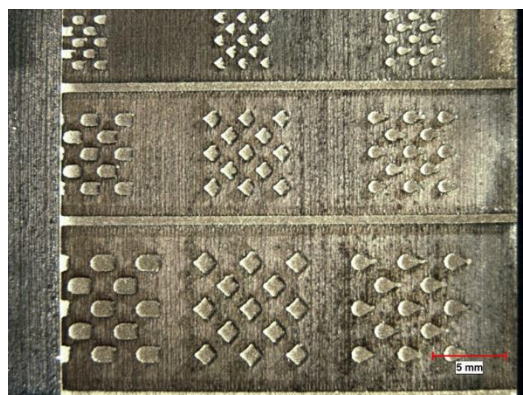
Generation 2



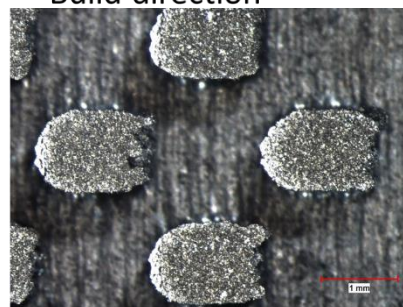
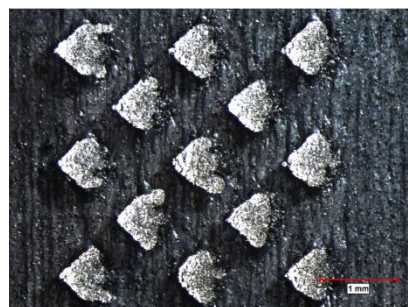
Generation 3



Improved powder remove processes revealed cleaner and more precise capabilities

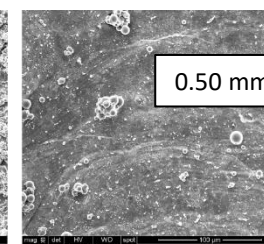
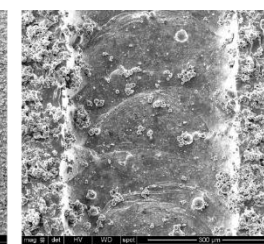
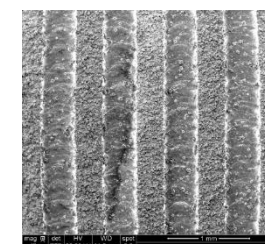
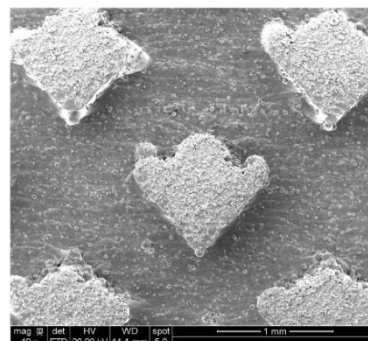
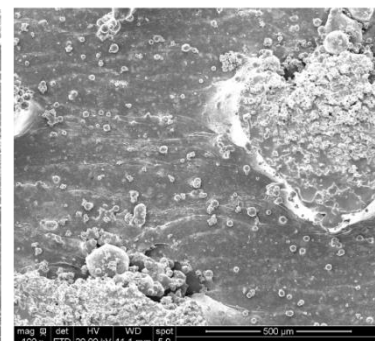
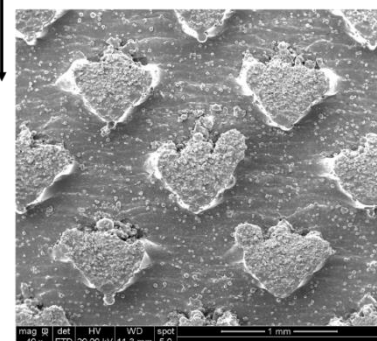


← Build direction

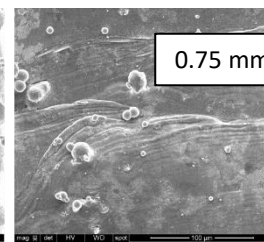
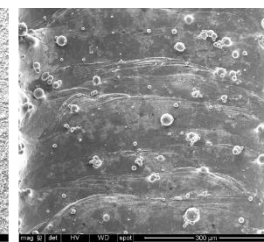
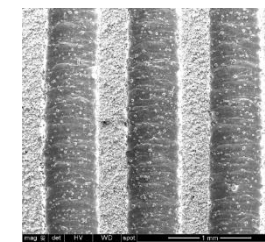


← Build direction

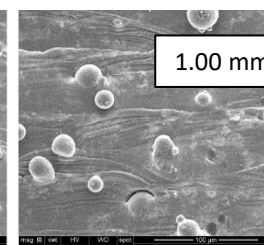
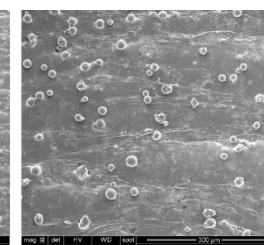
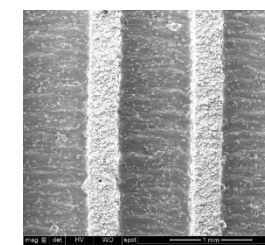
Build direction



0.50 mm passages

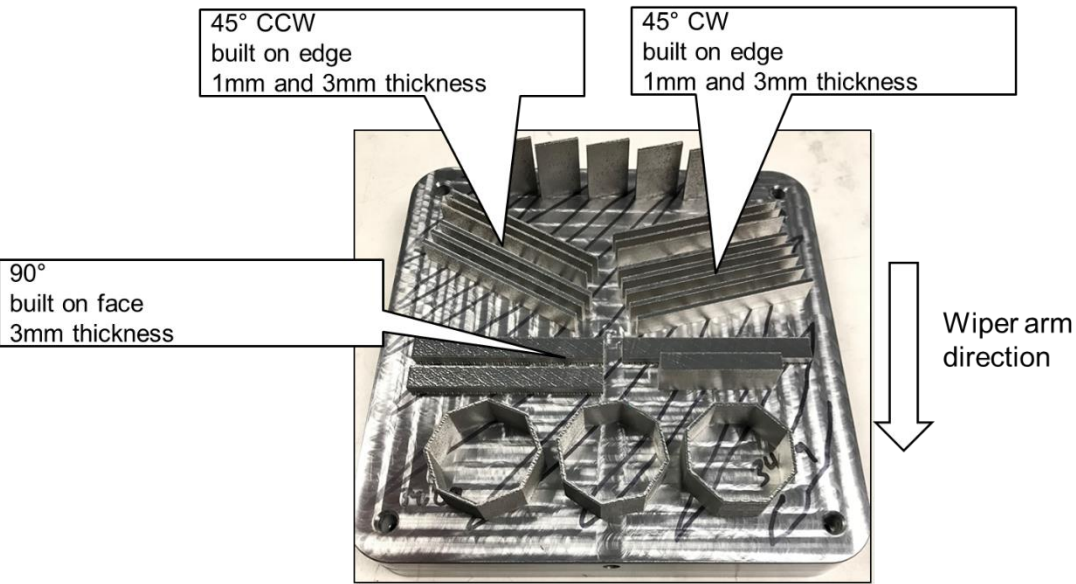


0.75 mm passages



1.00 mm passages

Two separate heat treatments and different build orientations studied

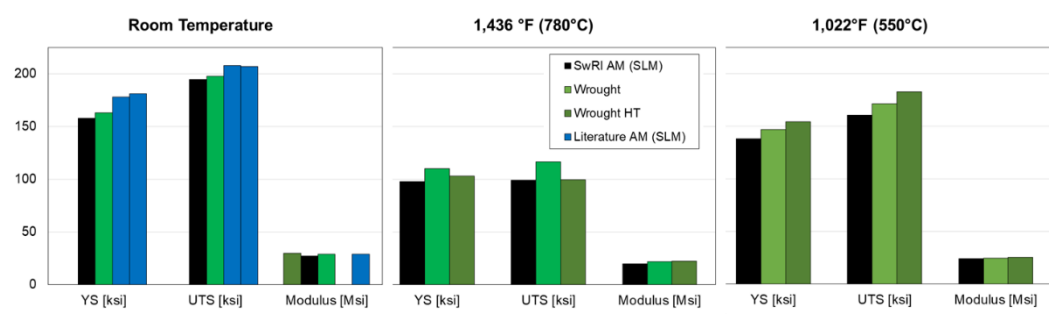


Process	#1	#2
Description	Combined HIP+Heat Treat	Separate HIP and Heat Treat
HIP Vendor (std)	Quintus (ASTM F3055-14a)	KittyHawk (ASTM F3055-14a)
Heat Treat (HT) Vendor (std)	Quintus	Texas Heat Treat (AMS 5663N)
HIP process	>14.5 ksi @ 2050°F-2165°F ±25°F for 4h ±1h hold in inert atmosphere; Cool below 800°F	
Solution HT process	1725°F-1850°F hold within ±25F for time commensurate with cross-sectional thickness. Cool at a rate equivalent to air cool or faster	
Aging HT process	1325-1400°F ±15°F hold for 6h ; Cool 100°F ±15°F per hr to 1150-1200°F; Hold ±15°F for 2h and air cool.	1325-1400°F ±15°F hold for 8h; Cool 100°F ±15°F per hr to 1150-1200°F; Hold ±15°F for 8h and air cool. May furnace cool at any rate provided the time at 1150-1200°F is adjusted to give 18h total

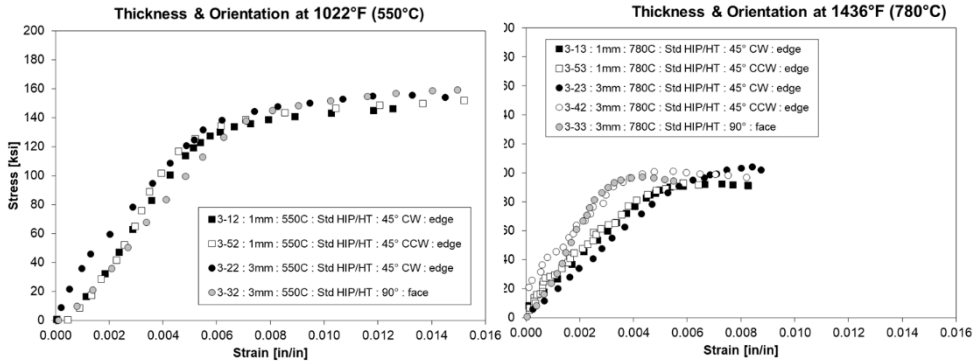
ID #	Part Description
3-11	1mm thick tensile coupon, built on edge 45deg CW Rotation
3-12	1mm thick tensile coupon, built on edge 45deg CW Rotation
3-13	1mm thick tensile coupon, built on edge 45deg CW Rotation
3-21	3 mm thick tensile coupon, built on edge 45deg CW Rotation
3-22	3 mm thick tensile coupon, built on edge 45deg CW Rotation
3-23	3 mm thick tensile coupon, built on edge 45deg CW Rotation
3-31	3 mm thick tensile coupon, built on face No Rotation
3-32	3 mm thick tensile coupon, built on face No Rotation
3-33	3 mm thick tensile coupon, built on face No Rotation
3-41	3 mm thick tensile coupon, built on edge 45deg CCW Rotation
3-42	3 mm thick tensile coupon, built on edge 45deg CCW Rotation
3-43	3 mm thick tensile coupon, built on edge 45deg CCW Rotation
3-44	3 mm thick tensile coupon, built on edge 45deg CCW Rotation
3-45	3 mm thick tensile coupon, built on edge 45deg CCW Rotation
3-51	1mm thick tensile coupon, built on edge 45deg CCW Rotation
3-52	1mm thick tensile coupon, built on edge 45deg CCW Rotation
3-53	1mm thick tensile coupon, built on edge 45deg CCW Rotation



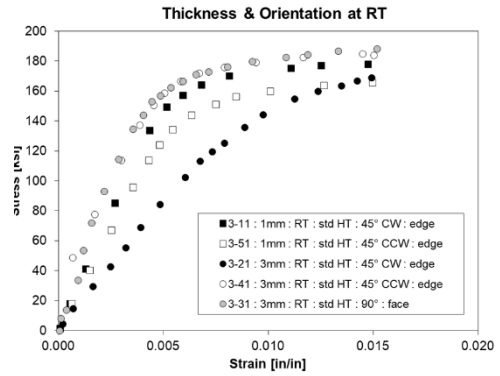
Orientations and heat treatments do show some sensitivity



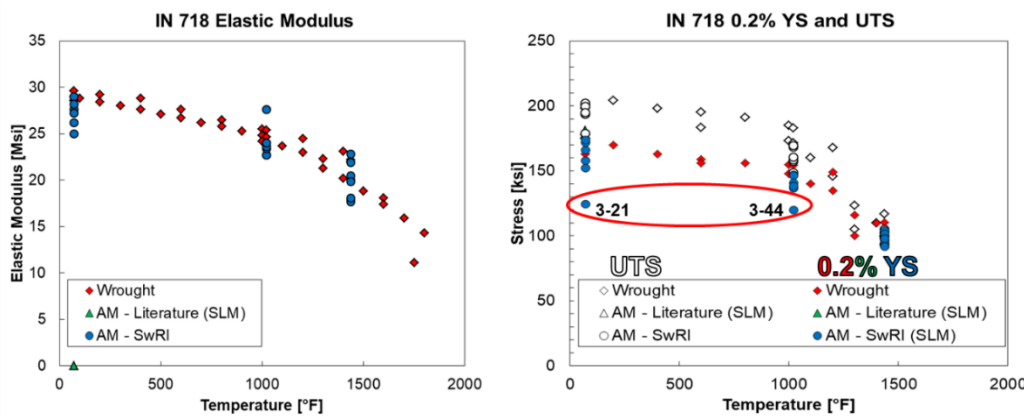
SwRI AM printed materials are typically within 10% of wrought properties and early estimates.



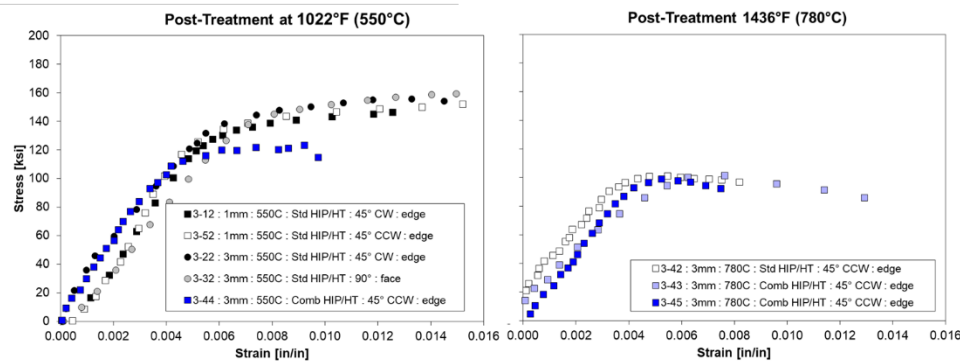
Effects of build orientation and thickness can be neglected at elevated temperatures.



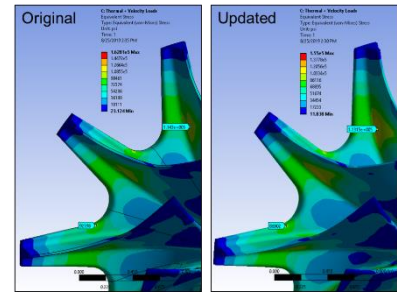
Build orientation and thickness can show sensitivity



The printed materials are consistent with literature and wrought properties for all temperatures.

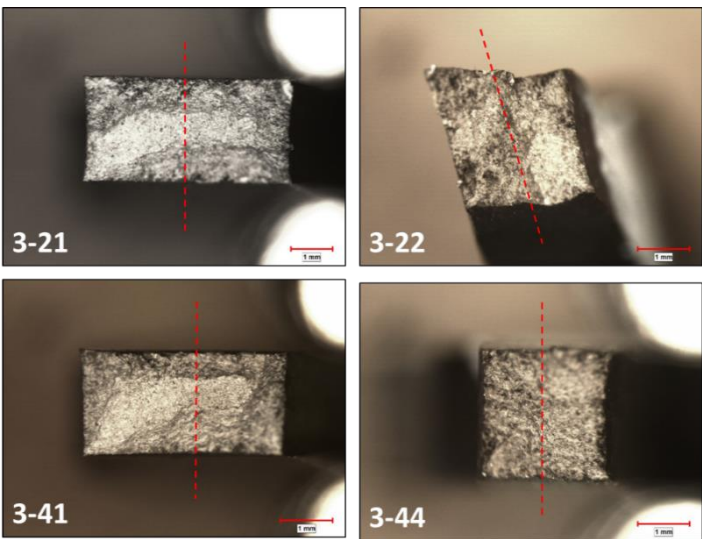


Post-treatment has little effect on material response at 780°C, but YS at 550°C is lower for the combined HIP/HT process.

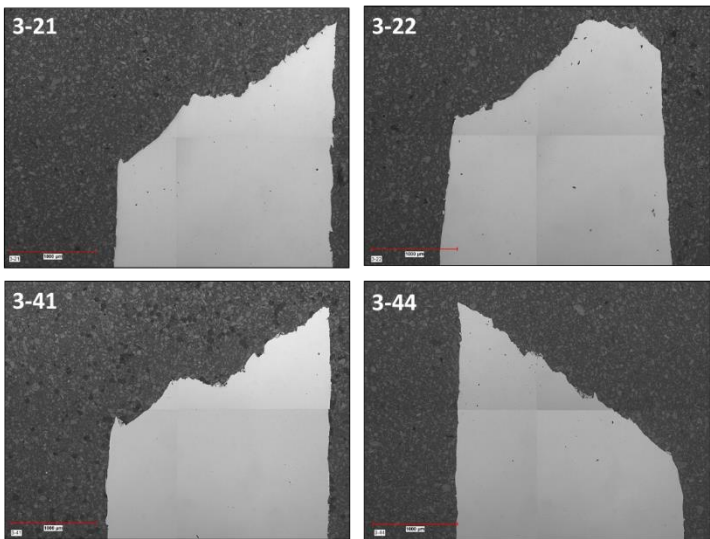


Don't forget to update analysis predictions with the new data!

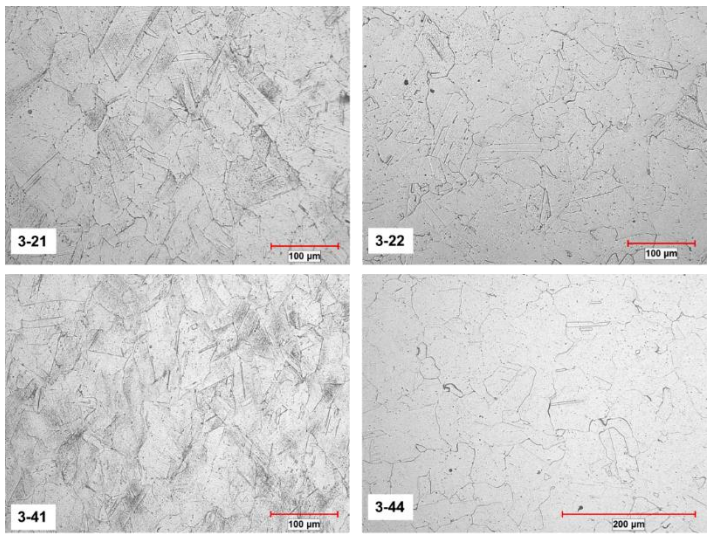
Deeper investigations made to examine anomalies



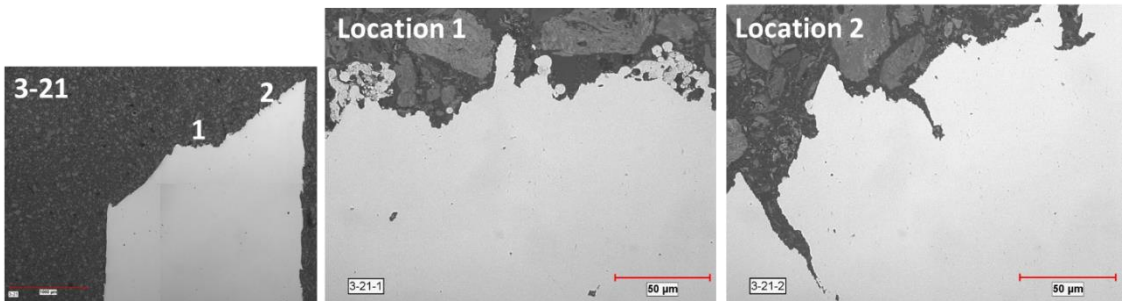
The specimens were sectioned at the fracture location for analysis.



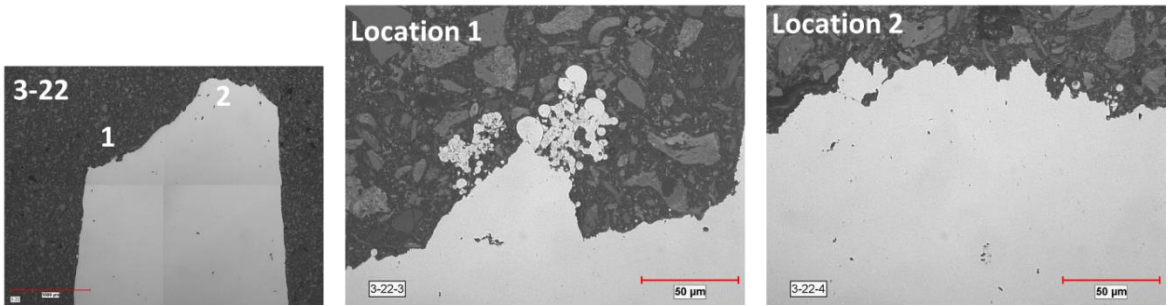
3-41 has least porosity.



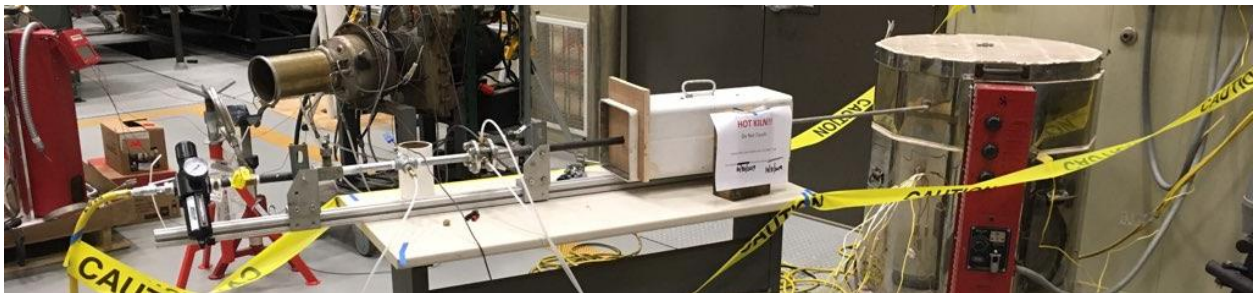
No significant differences in microstructure were observed in the specimens.



Specimen 3-21 exhibited areas of melting and partial fusion along the fracture surface.



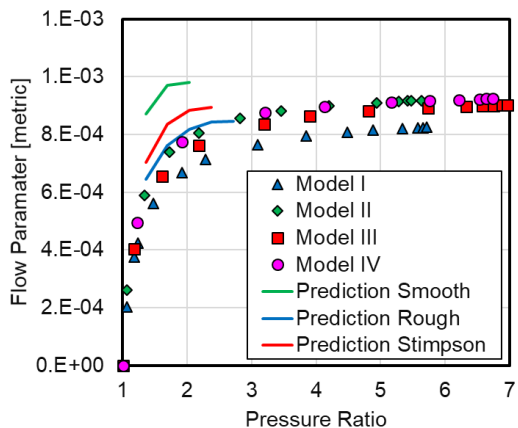
Enhanced images of the fracture surface of specimen 3-22, 3-44, and 3-41 did not indicate significant secondary cracking.



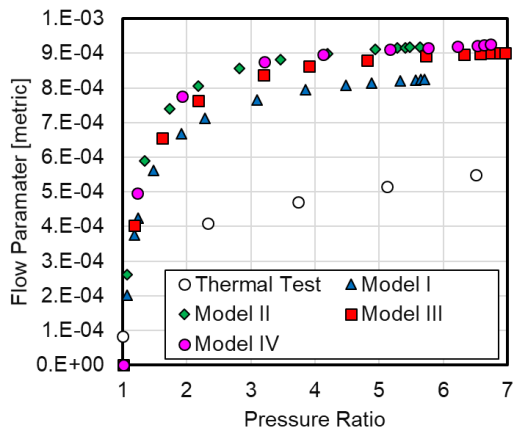
Build orientation and thickness can show sensitivity



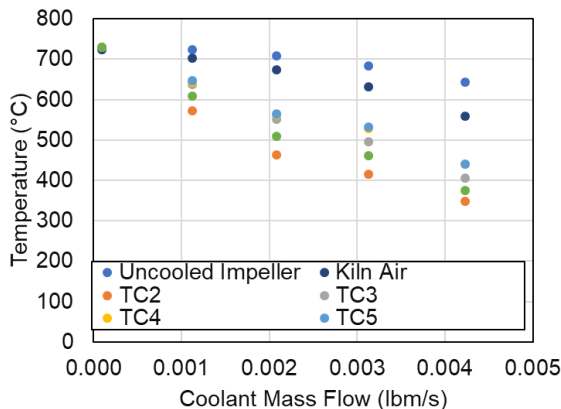
One impeller was cooled while the other impeller in the kiln served as a baseline.



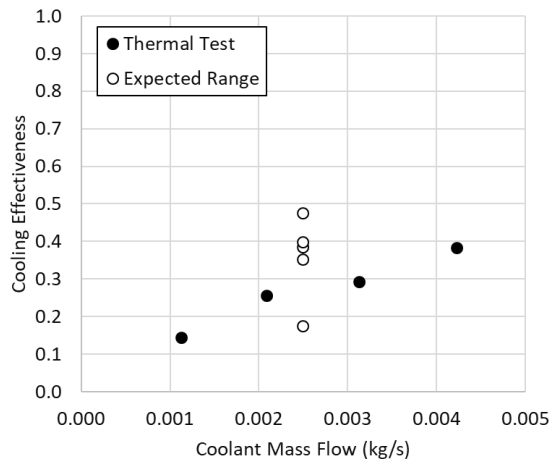
Impeller models II through IV had good flow agreement and all impeller tests indicated higher than expected surface roughness.



The flow in the thermal test was much lower than measurements recorded while the impellers were on the build plate.



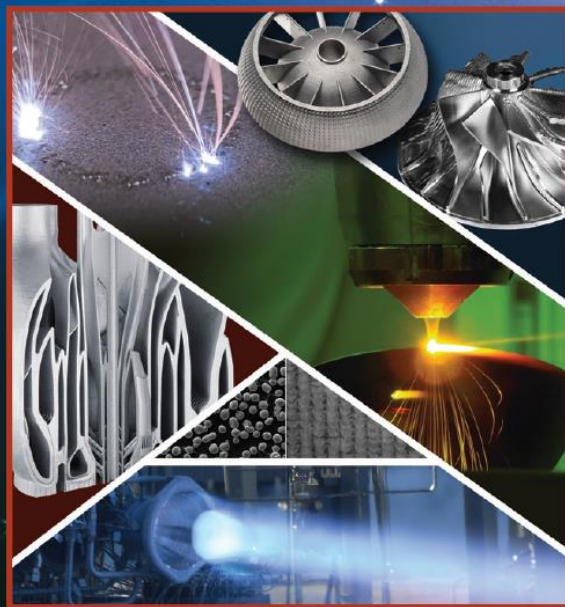
Increasing the mass flow lowered the temperatures of both impellers, as expected.



The cooling effectiveness measured in the thermal test is within the expected range of the one-dimensional thermal design calculations.

Metal Additive Manufacturing for Propulsion Applications

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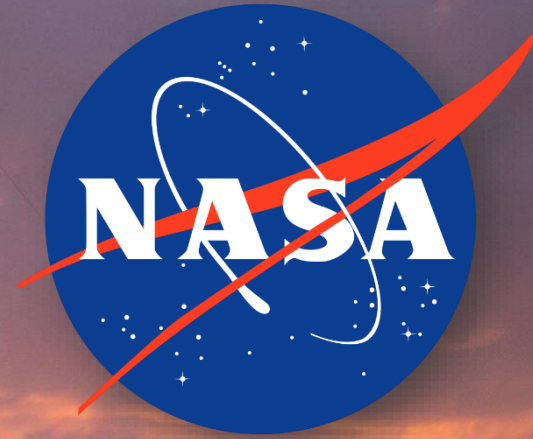
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Additive manufacturing (AM) processes are proving to be a disruptive technology and are grabbing the attention of the propulsion industry. AM-related advancements in new industries, supply chains, design opportunities, and novel materials are increasing at a rapid pace. The goal of this text is to provide an overview of the practical concept-to-utilization lifecycle in AM for propulsion applications.



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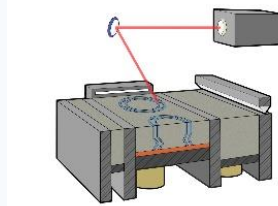
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Chapter 1

Introduction and
Applications of Additive
Manufacturing for
Propulsion



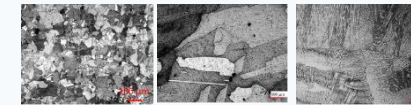
Chapter 2

Metal Additive
Manufacturing
Processes and Selection

Properties	Availability	Economics
<ul style="list-style-type: none"> Mechanical <ul style="list-style-type: none"> Tensile Yield Chop Hardness Other Physical <ul style="list-style-type: none"> Density Thermal Expansion Thermal Conductivity Welding Point Environment <ul style="list-style-type: none"> Corrosion Resistance Hydrogen Environment Chemical Resistance Fluid Compatibility 	<ul style="list-style-type: none"> Powder Supply Chain <ul style="list-style-type: none"> On hand Off the shelf Stock Special Powder Processing <ul style="list-style-type: none"> Regulatory restrictions Material processing requirements Machine Capability/Part Quality Known Build Parameters 	<ul style="list-style-type: none"> Material Cost Machine Build Time Anticipated Service Life Post processing financial Reusability Thermal Treatment

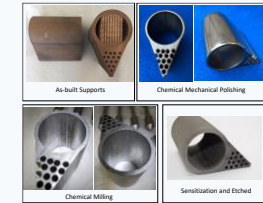
Chapter 3

Selection and Overview
of Additive
Manufactured Metals
and Metal Alloys



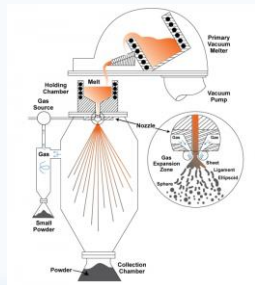
Chapter 4

Microstructure and
Properties of
Additively
Manufactured Metal
Alloys



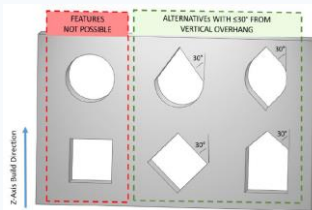
Chapter 5

Post-Processing of
Metal Additively
Manufactured
Components



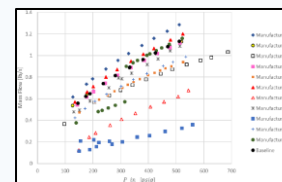
Chapter 6

Feedstock for Metal AM



Chapter 7

Functional Design
for Metal Additive
Manufacturing



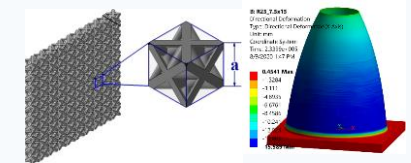
Chapter 8

Component
Performance and
Application
Characteristics



Chapter 9

Certification of Metal
Additive Manufacturing:
A NASA Perspective



Chapter 10

Emerging Additive
Manufacturing
Technology for
Propulsion